

Design and Analysis of
Accelerated Reliability Tests
with Piecewise Linear Failure
Rate Functions

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Problem Solving Tools




DART Abstract

- Part 1 proposes piecewise linear failure rate (PLFR) functions, for modeling simplicity and resemblance to the left-hand end of the bathtub curve. It shows how to estimate the PLFR, reliability, infant mortality, and MTBF. It proposes acceleration alternatives, including one that accelerates testing greatly.
- Part 2 describes how to design and analyze accelerated reliability tests, assuming a piecewise linear failure rate function and power law acceleration. It shows how to obtain credible results, with limited sample size and test time, *at one accelerated stress level*. It provides estimators for parameters, reliability, MTBF, confidence intervals, and it shows how to test model assumptions and verify MTBF. It is inspired by the observation that failure rates are not constant, often because of infant mortality.




Part 1 Contents

- Motivation for PLFR
 - MTBF and reliability for PLFR
 - Acceleration of PLFR and RAF
- 




Vision Statement

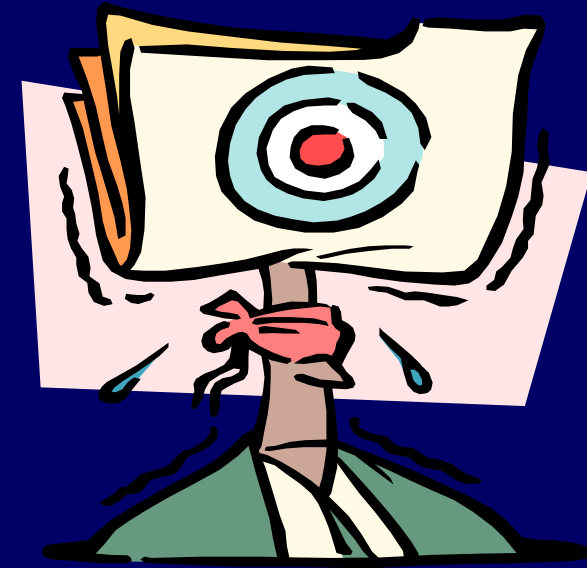
- Know and use reliability, “the probability of successful function [according to customers] to specified ages [DoA, warranty, PM, useful life] under specified conditions [field conditions].”
 - Management wants reliability before field data are available
 - So predict and test
 - ***No fair to say you don't have ages at failures! [<http://www.fieldreliability.com>]***
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DART Objectives

- Make *credible* MTBF, reliability, and failure rate function estimates
 - (*Credible Reliability Prediction*, <http://www.asq-rd.org/publications.htm> and <http://www.fieldreliability.com/Preface.htm>)
 - Quantify infant mortality
 - Verify MTBF
 - Use accelerated tests with only one, high stress level
 - Use available information early in life cycle
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Today's Situation?

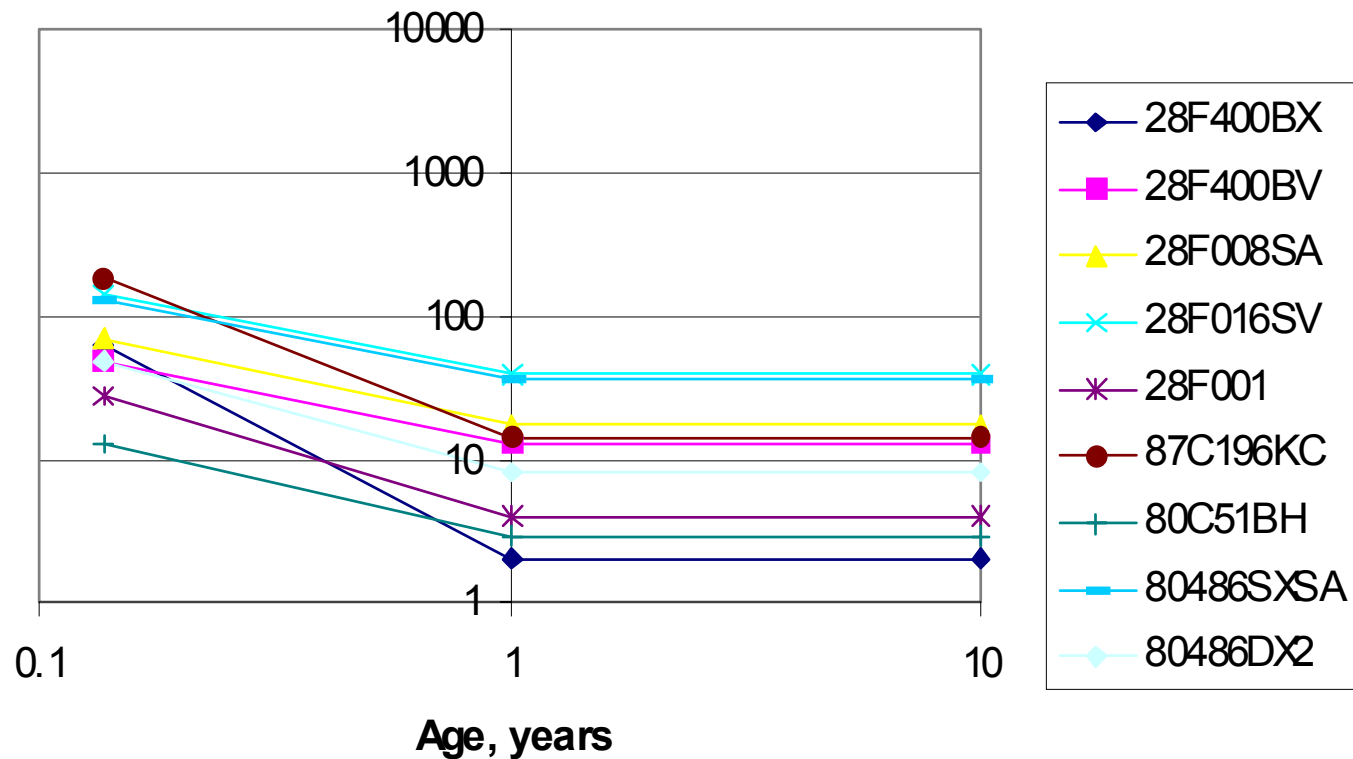


- Verify MTBF with tests that end \ll MTBF, even accelerated, without failures?
- Verify $P[\text{Life} > \text{useful life}] > 0.9$ with high confidence with small samples and short tests?
 - Does management ever agree to statistical sample size and test time?
- Extrapolate accelerated tests, at high stress, to working stress, with few failures \ll MTBF?
 - NIST [<http://www.itl.nist.gov/div898/handbook/index.htm>] ASQ [Meeker and Hahn], and others [Nelson, Bagdonavicius et al, Viertl] recommend at least two accelerated stress levels

Intel FITS have IM

Data used to be at

<http://www.intel.com/support>

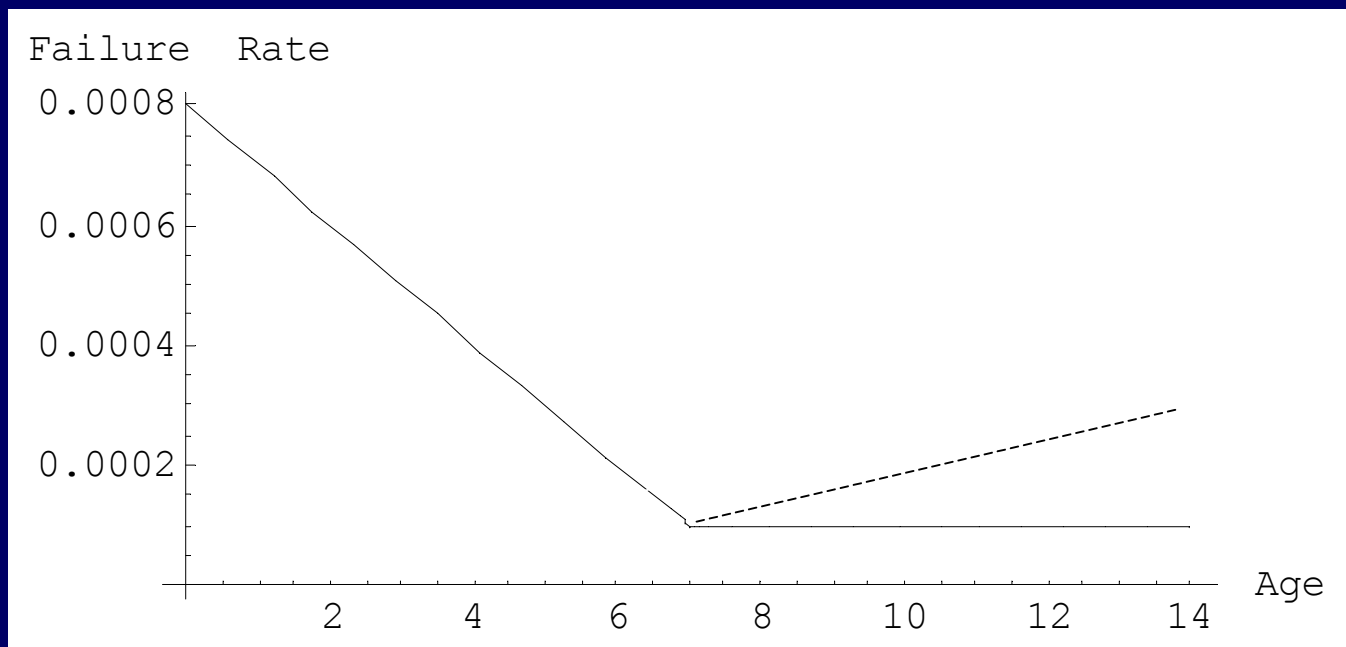


Invalid Assumptions

- Constant failure rate
 - Products have infant mortality, initially \downarrow failure rate.
- Monotonic \uparrow or \downarrow failure rate
 - Products often have both (rules out Weibull) [George 1995]
- Acceleration doesn't affect Weibull shape parameter
 - It does, usually
[\[http://www.esc.auckland.ac.nz/Organisations/ORSNZ/Newsletters/dec99.pdf\]](http://www.esc.auckland.ac.nz/Organisations/ORSNZ/Newsletters/dec99.pdf)
- Can't extrapolate to normal stress with only one accelerated stress level (one hand clapping)
 - We will.

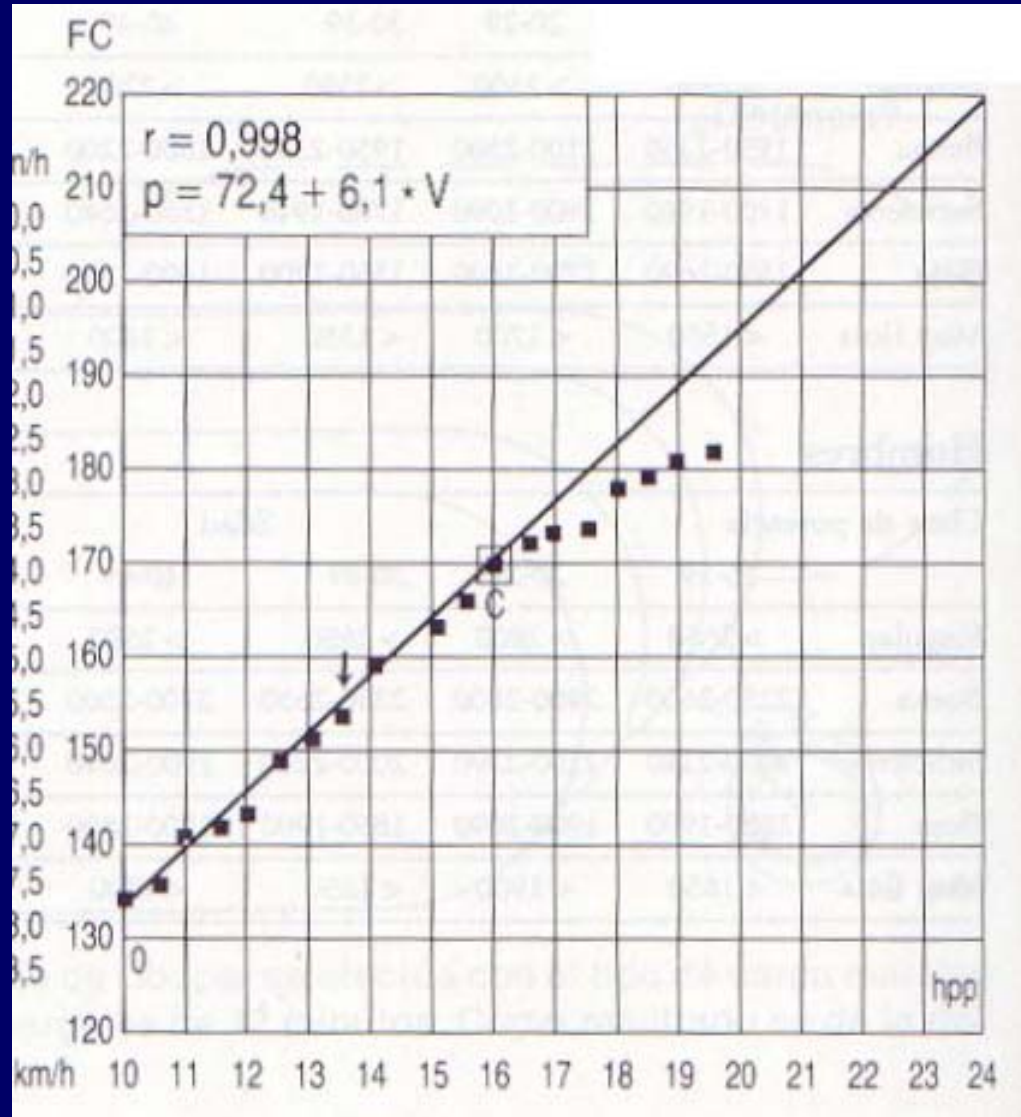
Piecewise Linear Failure Rate

- $a(t) = 0.0001 + 0.0001(7-t)^+$
- Dotted line is a possibly \uparrow failure rate



Test Conconi

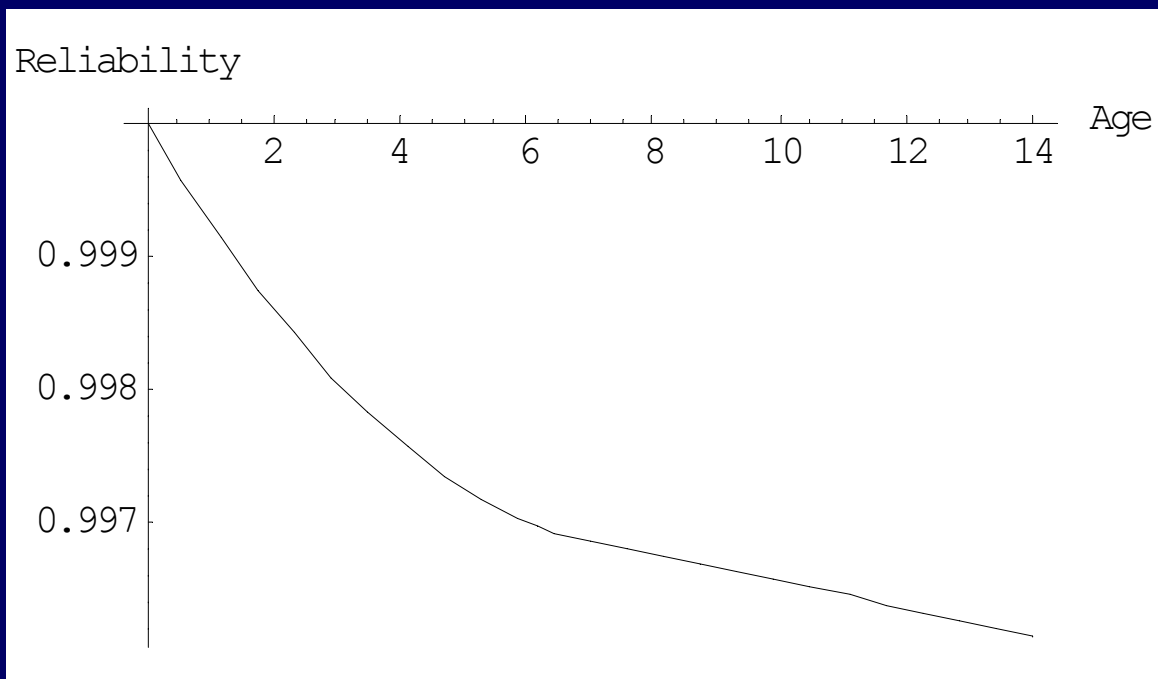
- Aerobic threshold is the heart rate at which the slope of work rate vs. heart rate decreases



Reliability with PLFR


- Reliability function has two parts, IM and after:
 - $\text{Exp}[(0.0001t^2)/2 - t(0.0001 + 0.0001t_0)]$ for $t < t_0$
 $\text{Exp}[-0.0001t - (0.0001t_0^2)/2]$ for $t \geq t_0$
 - $P[\text{Fail in IM}] \sim bt_0^2/2$

$$\text{MTBF} \sim (1 - t_0^2b)/2 + t_0^2b/6 - at_0^4b/24 = 9975.5$$

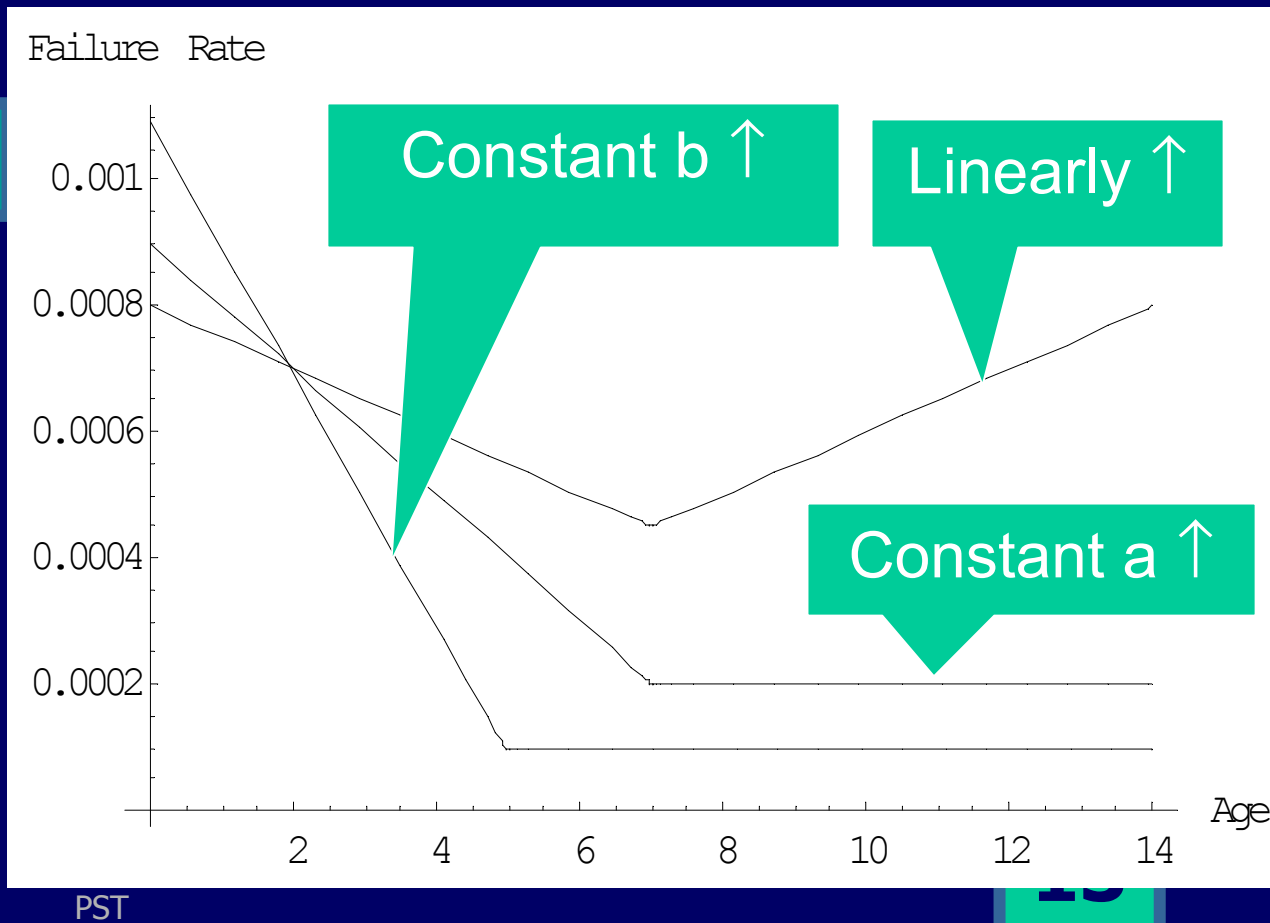




Acceleration alternatives

- Constant segment increases to greater constant
 - Constant segment becomes linearly increasing; acc. induces premature wearout, (limit of step stress)
 - IM Slope increases and perhaps t_0 , the age at the end of IM, decreases as acc.exacerbates process defects
 - ***System acceleration is not same as part accelerations! (unless parts are iid in series)***
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Acceleration alternatives



Reliability Acceleration Factor

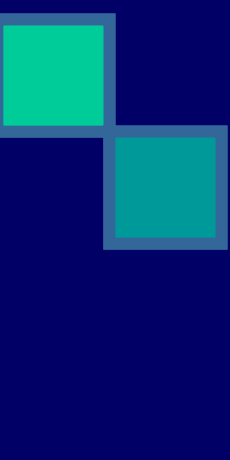
- $RAF(t) = (1-R_{Unacc}(t))/(1-R_{acc}(t))$
 - $RAF(60) = 1.705$ for double constant failure rate $2a$
 - $RAF(60) = 1.288$ for double infant mortality, b , increases from 0.0001 to 0.0002
 - $RAF(60) = 11.350$ for changing from constant, a , to linearly increasing failure rate, $a+0.0005t$

Fairly General Acceleration Model

- $a_{Acc}(t) = a_{UnAcc}[t/\theta(x)]/\theta(x)$ [Xiong and Ji]
 - $\ln\theta(x) = \alpha + \beta x$
 - x is stress factor, (stress-normal)/(max stress-normal)
 - Continuous version of step stress
- Multiplies failure rate by a factor and rescales age t
- Includes Arrhenius and Eyring models, [Shaked], motivated by Miner's rule
- Apply it to constant, IM slope, or entire piecewise linear failure rate function



Part 2

- Designs and examples
 - $|D|$ -optimal and other statistical designs
 - Moderately credible design
 - Need only one acceleration level
 - Examples: estimate parameters, LR test of MTBF
 - Unacc.
 - Acc.
 - Freebies
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Alternative Designs

- |D|-optimal is versatile, but recommends tests at $0, t_0$, and anywhere thereafter
 - DoE expects every design point to yield age at failure. Reliability tests often don't.
- Neyman design for multiple strata [Neyman, George 2002]
- Min variance design, must specify how much? [Nelson, Meeker and Hahn]
- Moderately credible design gives 50% probability of at least one failure in infant mortality and one thereafter, sufficient to estimate piecewise linear parameters

Moderately Credible Design

- 50% probability of ≥ 1 failure in IM and ≥ 1 after IM before end of test, t

Parameters	Case 1	Case 2	Case 3
a (guess)	0.01	0.01	0.01
b (guess)	0.01	0.01	0.01
t_0 (guess)	2	2	2
n (choose)	29	34	31
t (choose)	7	5.6	6.4
P[failure < t_0]	0.039	0.039	0.039
P[failure in [t_0 , t]]	0.047	0.034	0.041
P[failure < t_0 n]	0.371	0.356	0.366
P[≥ 1 failure in [t_0 , t] n-1]	0.739	0.680	0.718
P[Both, all]	0.501	0.499	0.504

Example Data

Sample	Age at failure	Survivors' ages
1	1	
2	2	
3	15	
4	30	
5	45	
6		45
19		45
20		45

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Example Result

Parameter/Model	a	$a+b(t-t_0)$	ct	$b(t-t_0)+ct$	a+ct	$a+b(t-t_0)+ct$
a	0.007	0.004			0.008	0.000
b		0.016		0.018		0.018
c			0.000	0.000	0.000	0.000
t_0		3.319		3.346		3.346
MTBF	154	215	73	83	125	84
In likelihood	-30.17	-28.21	-34.97	-27.78	-30.27	-27.78
LR statistic		3.919		14.389		4.989
Sig level		10%		10%		10%
χ^2		6.251		6.251		7.779

Best
model

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Put all your eggs in one basket for acceleration

- $a(t) = x^p(a + b(t_0 - t) + ct)$
- Test at highest reasonable stress
- Predict MTBF or use specification
- Find mle of parameters *constrained* to specified MTBF at working stress, $x=1$
- Use LR to test MTBF
 - $-2\ln[L(\text{MTBF})/L(\text{unconstrained})] \sim \chi^2$

Example Data

Sample	Age at failure	Survivors' age
1	1	
2	1	
3	2	
4	2	
5	10	
6	15	
7	20	
8	25	
9	30	
10	35	
11	40	
20		45


Example Result, $x = 1.5$

Parameter	$x^p(a+ct)$	$x^p(a+b(t-t_0)+ct)$
a	0.001452	0
b		0.018298
c	7.79E-05	0.000180
t_0		3.345768
p	5.149690	5
MTBF	125	125
Log likelihood	-53.84	-56.17
LR test statistic		-4.65
Sig level		10%
Chi-square		9.23634

Better model



Switch Example


- Demonstrate MTBF > 39,500 hours with 75% confidence
 - Test 7 switches for 6 weeks (1008 hours) at 60° C with MTBF AF = 14.6 (Arrhenius) to give χ^2 LCL of ~39,000 hours
 - Xcvrs failed at 486 and 660 hours (16 xcvrs per unit), after IM
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Real Example Data

Parameter	Value
c	3.56E-8 per hour per hour
Stdev c	$c/\sqrt{(2n)} = 2.38E-9$ per hr ²
MTBF	$\sqrt{(\pi/2c)} = 6645$ hours
25 th %ile of MTBF	6584 hours
MTBF of 16 xcvr acc.	$\sqrt{(\pi/32c)} = 1661$ hours
25 th %ile of 16-xcvr MTBF	~1000 hours
25 th %ile of 16-xcvr MTBF, unacc.	1000*35 = 35,000 hours



Recommendations

- For simplicity, use the PLFR to approximate left-hand end of bathtub curve...
 - Approximate acceleration with power law, rescale age if necessary and if Miner's rule fits
 - Use one, high level of acc. and MTBF
 - Send data to me for free samples
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