

Lead-free Soldering Materials and Processes

Requirements to Make Them Work

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This presentation is only a summary

- RoHS Globally - Latest Update
- Materials - Components and Boards
- Solders - Lead-free Choices
- Lead-free SMT Process
- Preventing Defects in SMT
- LF Wave Soldering Process
- Preventing Defects in Wave Assembly
- LF Hand Soldering and Rework

The information contained in this presentation is accurate as per the industry information available at the time of this revision. Please obtain the latest information for your process needs since lead-free assembly requirements may change.

RoHS / WEEE Directives Re-Cap

- Reduce and eventually eliminate the use of prohibited substances at the source (RoHS)
 - Maximum permissible levels in a homogeneous material will be as follows:

■ Cadmium (Cd)	100 ppm
■ Mercury (Hg)	1000 ppm
■ Lead (Pb)	1000 ppm
■ Hexavalent chromium (Cr(VI))	1000 ppm
■ Polybrominated Biphenyls	1000 ppm
■ Polybrominated Diphenyls Ether	1000 ppm
- Recycle as much of the product as possible after its useful life, in order to minimize the issues of disposal (WEEE). Very much a recycling law.

Exempt / Out of Scope?



Products that are exempt include:

- Network infrastructure
- High-end computing equipment

Products that are out of the legislation's scope include:

- Medical equipment
- Aerospace equipment
- Defense electronics
- Products used in national security
- Automotive electronics (covered by ELV legislation)

Celestica presentation by Dan Shea, CMAP International Lead-free Conference,
Toronto, Canada May 2006.

Risks of Relying on Exempt / Out-of-scope Status



Reasons companies who are out of scope / facing exemption should act now include:

- Exemption applies to lead *in solder*, not other 5/6
- Conversion costs delayed, not avoided
- Longer design / product cycles = need to start now!
- Non-compliant component obsolescence
- Premium on obsolete components
- OEM green leadership / branding
- Competitor sets lead-free proof point...possible deadline shift!
- Products with temporary exemptions or out of scope may still be impacted as suppliers move away from leaded offerings

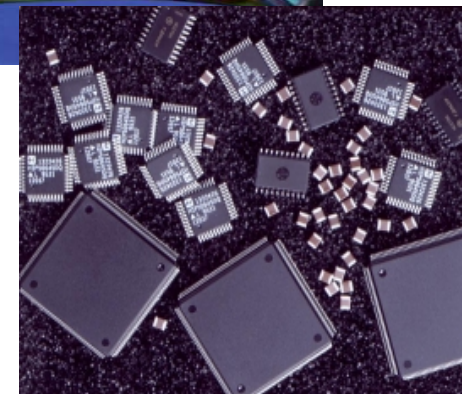
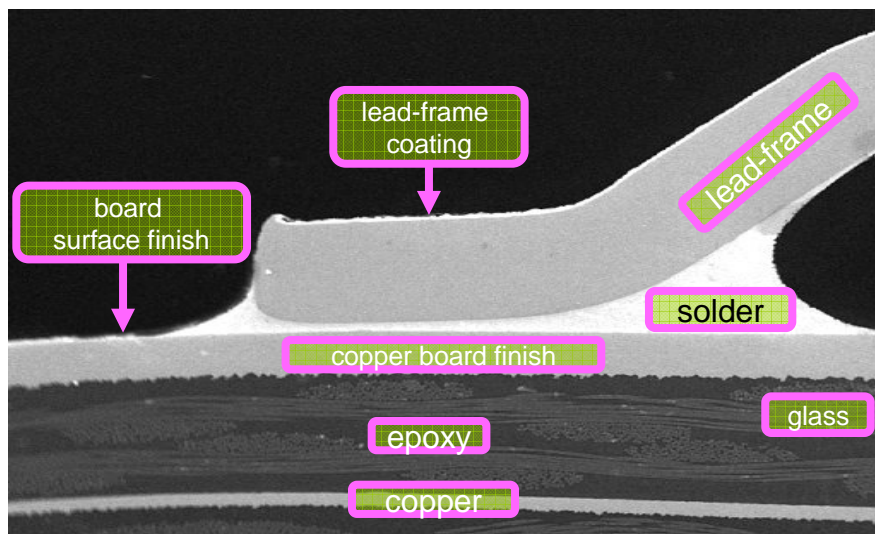
EC Stakeholder Consultation 2002/95/EC

Additional exemptions



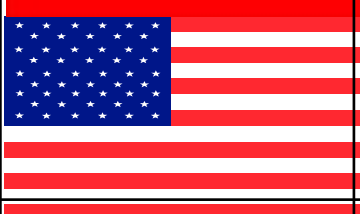

- Lead in tin whisker resistant coatings for fine pitch applications
- Solders containing Lead and Cadmium for special applications
- Lead in connectors, flexible PCB's, flexible flat cables
- Low melting point alloys containing lead
- Applications of lead, mercury, cadmium, hex.chrome, PBDE, PBB's in aerospace and aeronautical applications

RoHS Directive: Substance Limits

- Maximum Concentration Values in weight percent
 - 0.1% for Pb, Hg, hexavalent Cr
 - 0.01% for Cd
 - 0.1% for PBB and PBDE flame retardants
- Concentration is per **homogeneous material**
- **'Homogeneous material'** means a material that cannot be mechanically disjointed



Not Just Europe

	Regulation	Compliance Timing
	Reduction of Hazardous Substances (2002/95/EC)	July 2006
	Regulation for pollution control of Electronics Products (RPCEP)	March 2007
	California RoHS-equivalency measures 52 bills pending in 20 states	January 2007 Various
	JGPSSI Guidelines for Standardization of Material Declaration JEITA Lead-free Roadmap	July 2003 End 2005 for assemblies

Presented at the International Lead-free Conference, Toronto, Canada, May 2006.



Integrated Supply Chain

Industry Challenges with China Environmental Product Regulations

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Raleigh, USA
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ON DEMAND
SUPPLY CHAIN

| May 29, 2006

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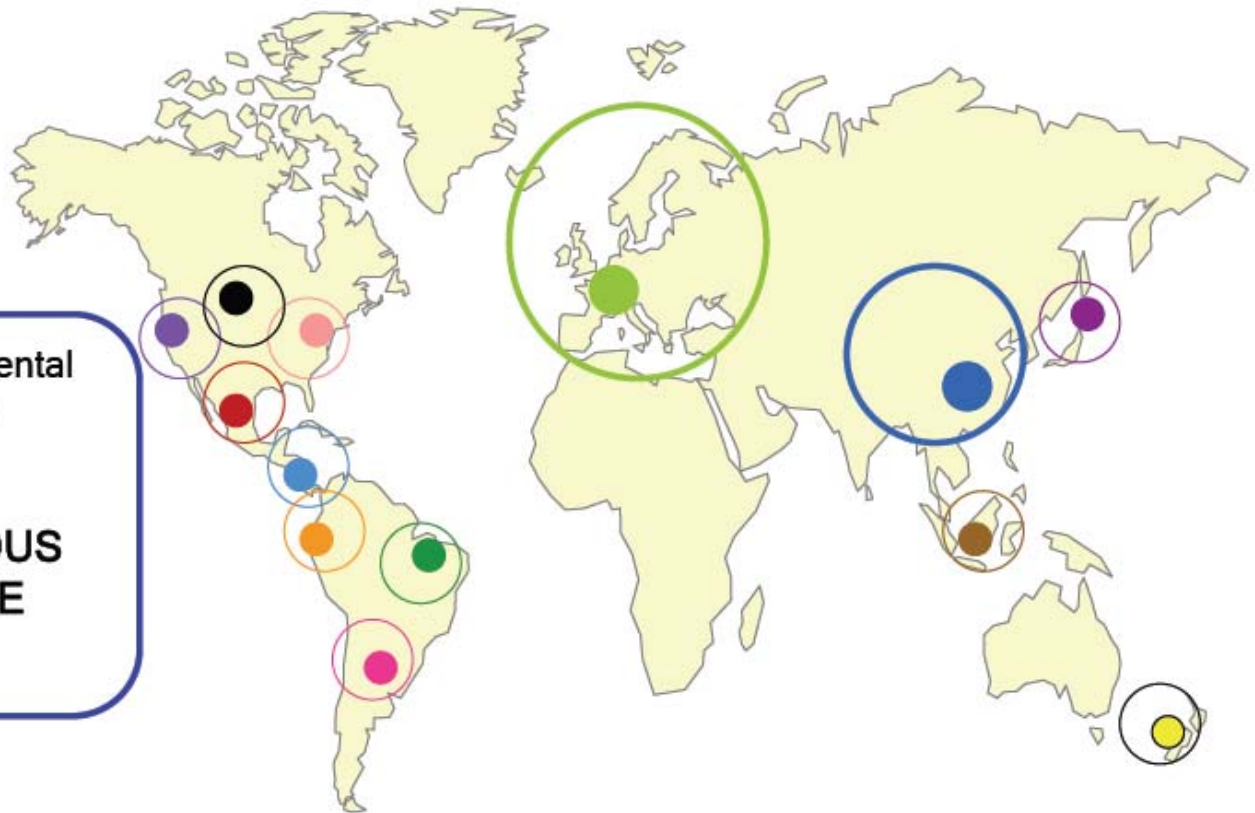
- The 6 standards are identified as **PRC Electronics Industry Standards**:
 - Marking / Labeling Requirements
 - Maximum Concentration Value (MCV) Limits
 - Hazardous Substance Testing Requirements
 - Pb-free Solder Materials
 - Product Catalogue Definition
 - Certification Requirements



Global Electronics Market

Currently, many different environmental regulations are emerging globally - based on:

**RESTRICTION OF HAZARDOUS
SUBSTANCES & END OF LIFE
TAKE BACK**



Europe:

China:

Korea:

Canada:

United States:

Americas:

European Union WEEE & RoHS Legislation

Management Methods for Controlling Pollution

Act for Resource Recycling of Electronic Products and Automobiles

Provincial Regulations in 7 provinces

State Regulations in 37 states

Mexico, Columbia, Brazil, Costa Rica, Argentina, Paraguay, Uruguay

Press-Release In the News, November 2006, California regulation.

SACRAMENTO – The **California Department of Toxic Substances Control** will hold a public workshop this week to solicit input and update stakeholders on the development of regulations prohibiting the sale of non-RoHS compliant electronic devices in California.

The workshop will be held Nov. 9, at the CalEPA Building in Sacramento. A remote videoconference will take place in Glendale, CA. All interested parties are invited to participate.

Email Linda Sargent at lsargent@dtsc.ca.gov or Cindy Chain-Britton at cchainbr@dtsc.ca.gov, or call 916-323-9219.

The event will also be accessible via a live audio webcast on the Cal/EPA website at <http://www.calepa.ca.gov/broadcast/>. Questions and comments may be submitted in real time and will be considered when DTSC finalizes the regulation proposal.

Beginning in 2007, a California law will ban the sale of some electronic devices that contain certain hazardous substances. The Electronic Waste Recycling Act (EWRA), which was signed into law in September of 2003, requires the DTSC to adopt regulations to prohibit covered electronic devices “from being sold or offered for sale” in California if they are prohibited from sale in the European Union under the RoHS Directive because they contain certain heavy metals.

As of December 2005, DTSC had identified eight categories of covered electronic devices in its regulations. The list of covered devices includes:

1. Cathode ray tube containing devices (CRT devices)
2. Cathode ray tubes (CRTs)
3. Computer monitors containing cathode ray tubes
4. Laptop computers with liquid crystal display s
5. LCD-containing desktops
6. Televisions containing cathode ray tubes
7. Televisions containing LCD screens
8. Plasma televisions.

The EWRA will restrict the use of lead, mercury, cadmium, and hexavalent chromium in electronic devices sold in California. The RoHS Directive was amended on Aug. 18, 2005, to add maximum concentration values for the six restricted substances. DTSC will incorporate the EU's MCVs for lead, mercury, cadmium, and hexavalent chromium in its regulations implementing the EWRA.

DTSC's RoHS regulations will recognize any exemptions adopted by the EU for the use of lead, mercury, cadmium, or hexavalent chromium that apply to covered electronic devices. DTSC will present the proposed RoHS regulations and solicit comments and suggestions from attendees.

Summary

Key Procurement Issues for RoHS

- Components
- Boards
- Solders and fluxes
- Wires and cables
- Metal fixtures and fasteners
- Plastic parts, casings etc...

Lead-Free – IPC/JEDEC Definition



Pb-free (lead-free):

Electrical and electronic assemblies and components in which the Lead (Pb) level in any of the raw materials and the end product is **$\leq 0.1\%$ by weight** and also meets any Pb-free requirements/definitions adopted under the RoHS Directive 2002/95/EC.

Important Note:

A 'Pb-free' component may not necessarily be compatible with Pb-free processing temperatures, as process-compatibility must be determined by the
“Maximum Safe Temperature”

JEDEC Standard JESD97 or IPC-1066

- Pb-free category:
 - Assigned to Pb-free components, boards, and assemblies indicating the general family of materials used for the 2nd level interconnect including solder paste, lead/terminal finish, and terminal material/alloy solder balls
 - e1: SnAgCu
 - e2: Other Sn alloys – no Bi or Zn (SnCu, SnAg, SnSb)
 - e3: Sn
 - e4: Pre-plated (Ag, Au, NiPd, NiPdAu)
 - e5: SnZn, SnZnx (no Bi)
 - e6: Bi
 - e7: Low Temp.< 150°C, In based, no Bismuth
 - e8, e9 unassigned
 - Tin-lead boards and components have no assigned label

e2

~~Pb~~

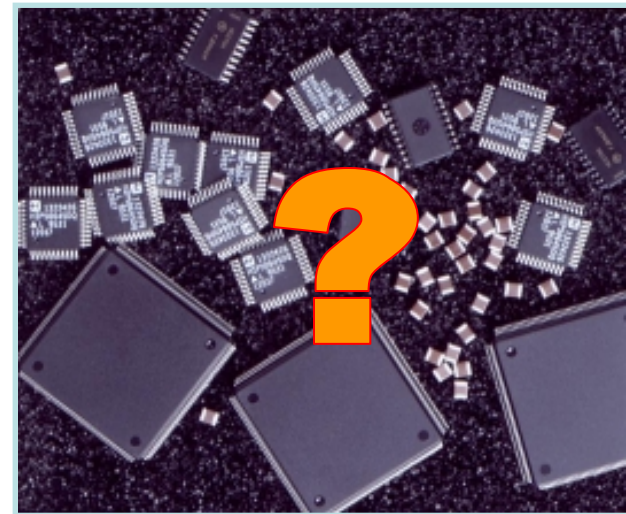
 TEXAS INSTRUMENTS		 G4		(1P) SN74LS07NSR	
MADE IN: Malaysia 2DC: 2Q:		(Q) 2000 (D) 0336			
MSL 2 /260C/1 YEAR		SEAL DT	(31T) LOT: 3959047MLA		
MSL 1 /235C/UNLIM		03/29/04	(4W) TKY (1T) 7523483SI2		
OPT:			(P)		
ITEM:		39	(2P) REV: (V) 0033317		
LBL: 5A (L)T0:1750			(20L) CS0: SHE (21L) CCO:USA		
			(22L) AS0: MLA (23L) ACO: MYS		



Choosing the Materials For Pb-free and Directives Compliance

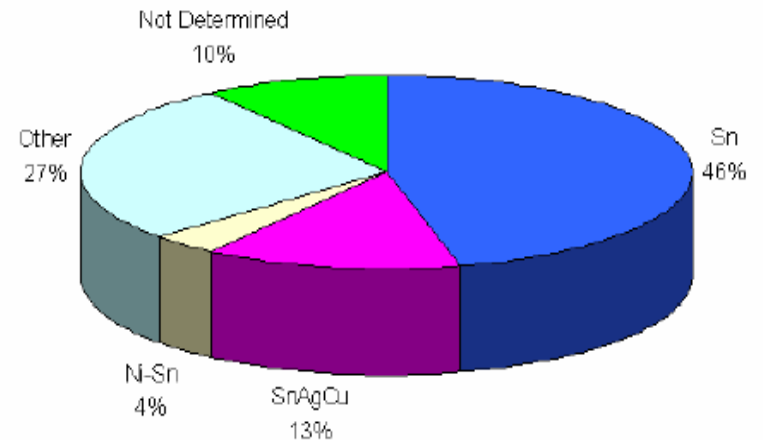
Summarizing the Key Points on Components

- Lead-free termination finish
- RoHS compliancy, metal finishes and plastics
- Thermal compatibility
- Moisture sensitivity rating



Component LF Finishes

Note: If your not transitioning do check
what you are getting.
Avoid surprises.

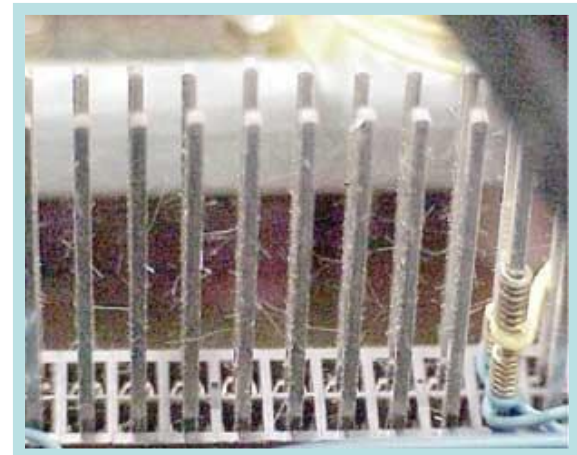


- Ni alloys: Ni/Kovar, Alloy 42, difficult to solder
- Pd/Ni: Palladium acts similar to Au – as a oxidation inhibitor, different metallic combinations available
- Pd/Ni/Ag Low ductility – Cracking a problem, More expensive
- Pd/Ni/Au Low ductility – Cracking a problem, More expensive
- SnBi: Can't mix with Pb, low mp phase at 97°C
- Pure Tin: Whisker potential, especially fine pitch components
- SnAg: Tight plating control required
- SnCu: Tight plating control required
- Many others finishes available

Ways to Prevent Tin Whiskers

- Add a small amount of Cu or Ag to tin
- Use of nickel barrier between copper and tin*
- Use matte tin(larger grain deposits), instead of fine grain bright tin finish
- Use of thicker tin coat 8-12 micrometers
- Reflow of surface prevents whisker growth
- Anneal process
- Newer anti-whisker fine grain matte tin finishes,
 - example Technic Advanced Technologies, TechStan EP

* Studies seem to indicate this to be the most effective way to minimize whiskers.



IPC/JEDEC J-STD-020C

Moisture/Reflow Sensitivity Classification for Nonhermetic Solid State Surface Mount Devices

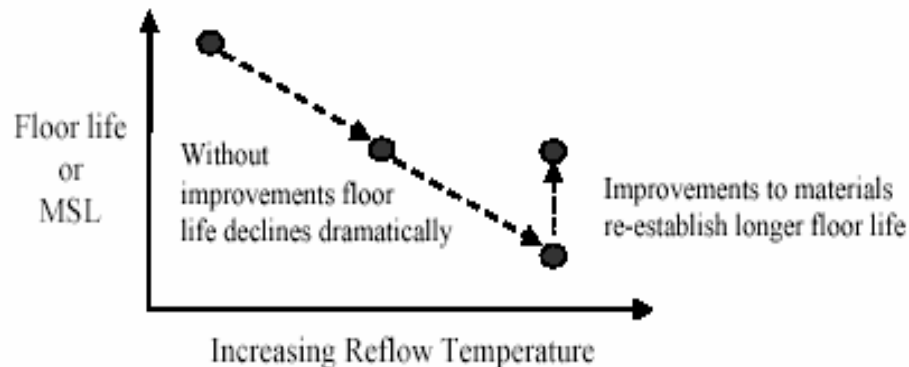
Higher processing temperatures for lead-free assembly increases risks of:

- Internal delamination
 - Internal cracks
 - Bond damage, die lifting, thin film cracking, popcorning
 - Cratering
 - External package cracks
-
- Establishes new lead-free max. processing temperatures
 - Minimum and Maximum thermal profile requirements
 - Moisture Sensitivity Level (MSL rating) classification criteria

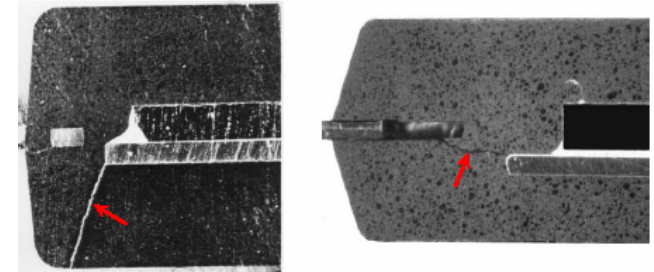
Impact of Lead-free on MSD

Results of Improvements to Materials (PBGAs)

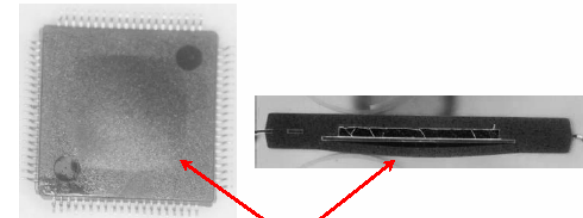
JEDEC Moisture Sensitivity Level		Previous Materials			New Pb-free Process Compatible Materials		
Level	Floor Life	225°C	240°C	260°C	225°C	240°C	260°C
2A	1 Month	Pass	Fail	Fail	Pass	Pass	Pass/Fail
3	1 Week	Pass	Pass	Fail	Pass	Pass	Pass
4	3 Days	Pass	Pass	Pass	Pass	Pass	Pass



“Popcorn Effect” Type I Crack

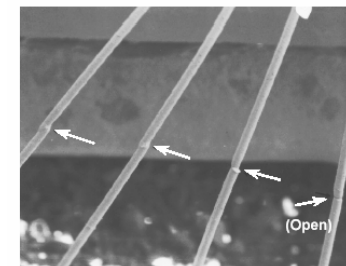


Package Warpage



Die Paddle Belly Bulge: LQFP

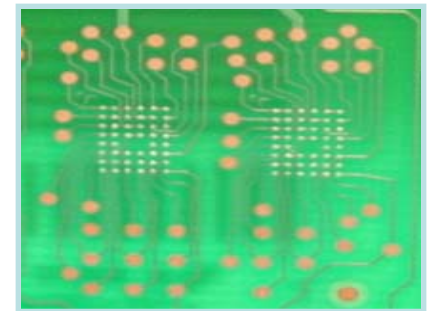
Bond Wire Damage



Wires sheared by package crack.

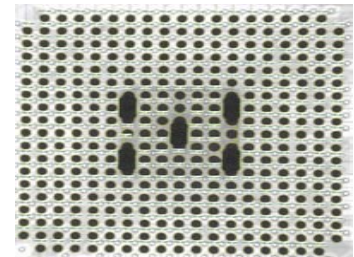
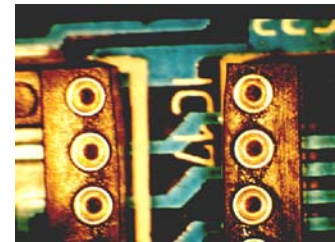
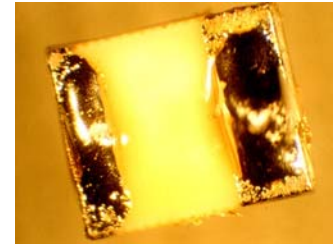
Summarizing Key Points on Boards

- Lead-free board finishes
- RoHS compliancy for laminates
- RoHS compliancy for solder mask
- Thermal compatibility, up to 260°C
- Changes to Tg and Td

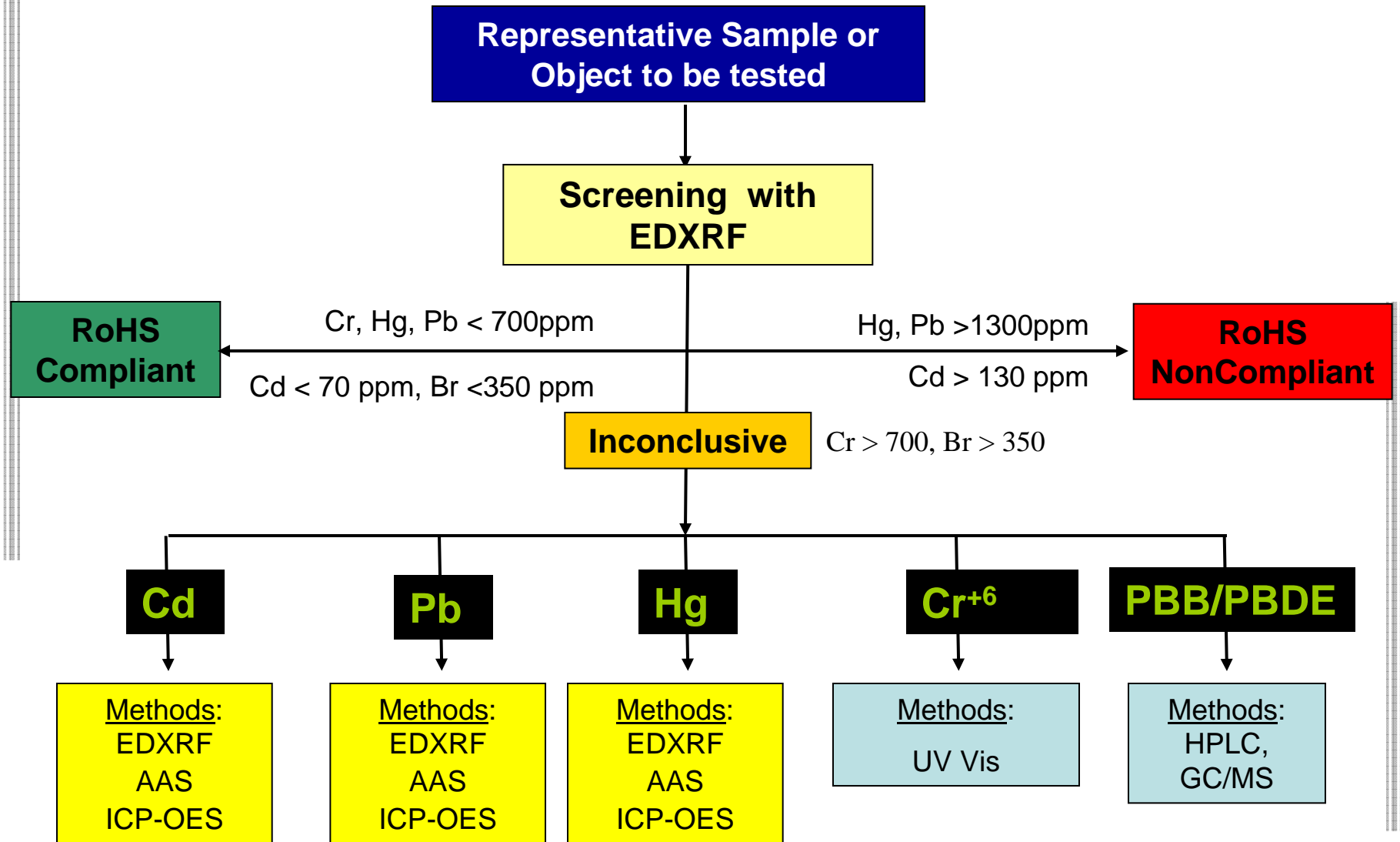


Component-Board Process Compatibility

- Termination and board finish choices
- Thermal compatibility
- Plastics, molding compounds for components, etc
- RoHS compliancy, all levels
- Moisture sensitivity levels of SMD's
- Availability, Cost
- Shelf-life and logistics



Proposed Test Flow Procedure for RoHS Substances



Electronic Related Applications XRF

- **“Due Diligence”**
 - Verify Certificates of Analysis and Supplier Declaration
 - Spot check your “high risk” vendors
 - Reduce amount of money spent on outside lab testing
- **Identification of prohibited material**
 - Analysis of Pb and other elements for prevention of tin Whiskers
 - RoHS Exempt products
 - *Medical*
 - *Military*
 - *Long-Life applications*



X-ray Fluorescence Unit



Lead-Free Solder Selection

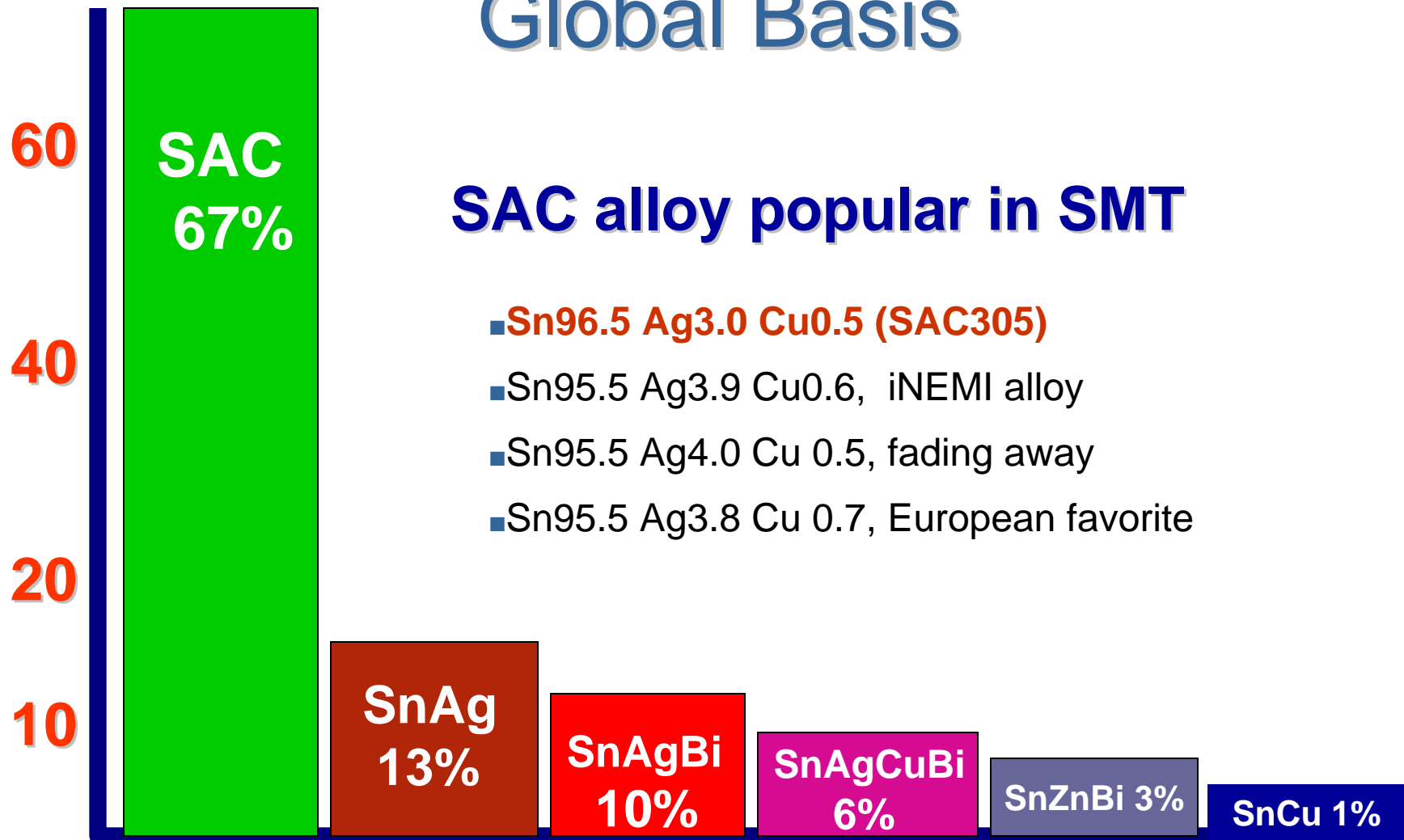
Alloy Selection Overview

- Alloy selection, choosing the solder to suit the end in mind
- Must consider MP, alloy strength, ductility, reliability data, availability, patents, etc.
- Current trends are toward SAC system for SMT
- Current trends are toward SAC or Sn/Cu system for wave soldering

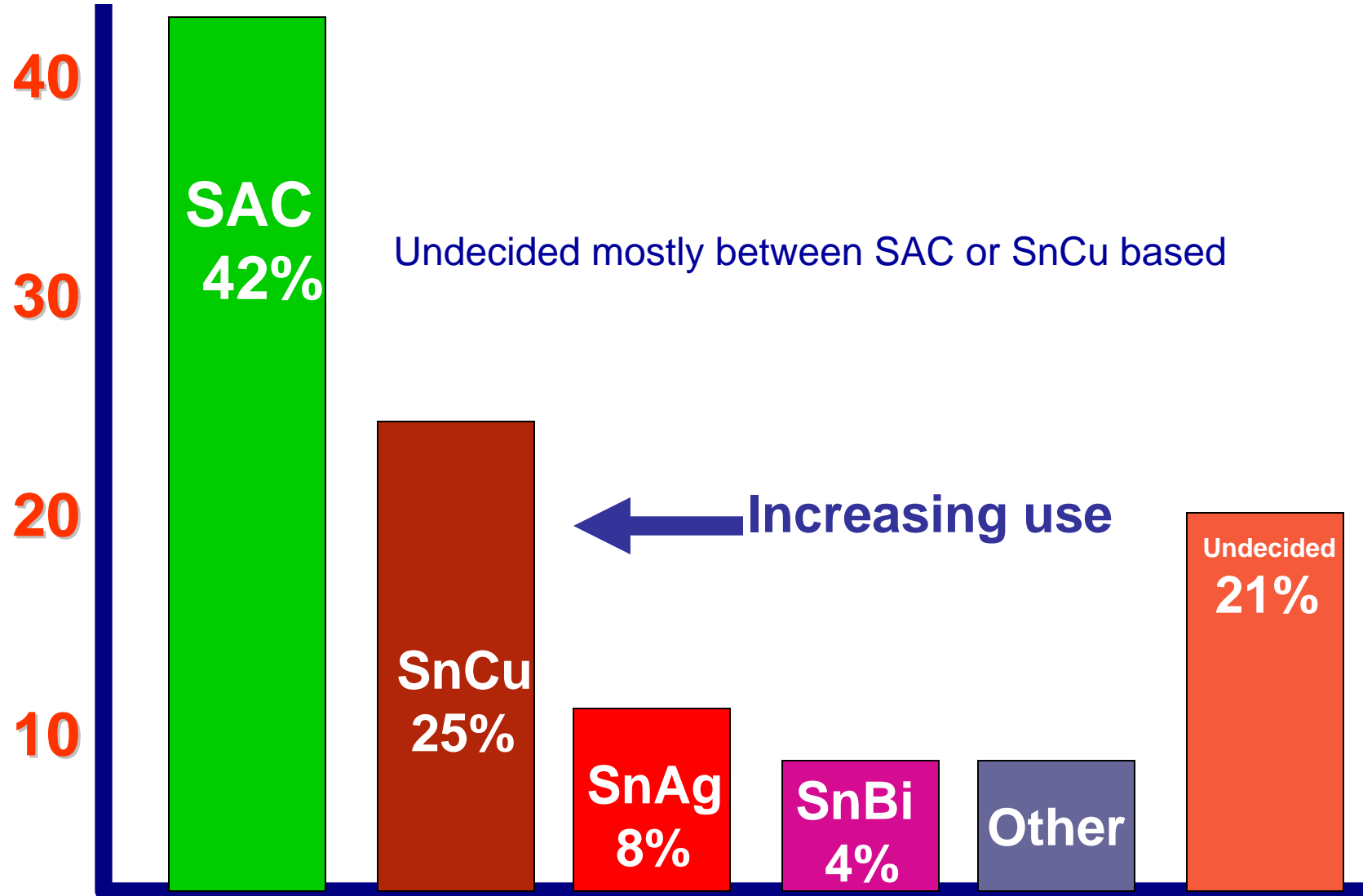
Common LF Alloys

- **SnAgCu (or “SAC”) family** (MP = ~217C)
 - Many available varieties with different proportions of Sn, Ag & Cu
- **Sn96.5 Ag3.5** (MP = 221C)
 - Sn/Ag Eutectic alloy
- **Sn99.3 Cu0.7 family** (MP = 227C)
 - Sn/Cu Eutectic alloy, plus Nickel or Germanium, Bismuth
- **Sn99 Ag0.3 Cu0.7** (MP = 217-227C)
 - Lower cost “SAC” alloy due to lower Silver content

Reflow Solder Selection on a Global Basis



Global Wave Solder Selection



SAC305 for Wave

- Sn96.5 Ag3.0 Cu0.5 (MP ~217C)
- Popular wave soldering alloy
- Highest cost
- More data available
- Good reliability
- Cosmetic issues

SAC0307 for Wave

- Sn99 Ag0.3 Cu0.7 (MP 217-227C)
- Lower-Silver version of traditional SAC alloys for lower cost
- Originally used as a plumbing solder, little data for electronics applications
- Could be worth considering in some applications as a replacement for SAC305 with lower cost

Sn/Cu based solders for Wave

- Sn99.3 Cu0.7 eutectic point of this binary system (MP 227°C)
- Low cost alternative to SAC305 for wave
- SnCu with additives, Nickel, Gallium, Cobalt, Bismuth
 - SnCuNi an option, several alloys here
 - These materials are lower in cost and reliability data is still being collected

Alloy Selection Rework

- Rework:
 - Match rework alloy to alloy used to produce original joint
- Other Hand Soldering:
 - Match alloy to whatever is already used on the board

Just a word on “Surface Shrinkage Effects”

As mentioned in J-STD-610D, Chapter 5

Typically seen with SAC solders in wave, selective and hand-soldering

5 Soldering

5.2.11 Soldering Anomalies – Hot Tear/Shrink Hole

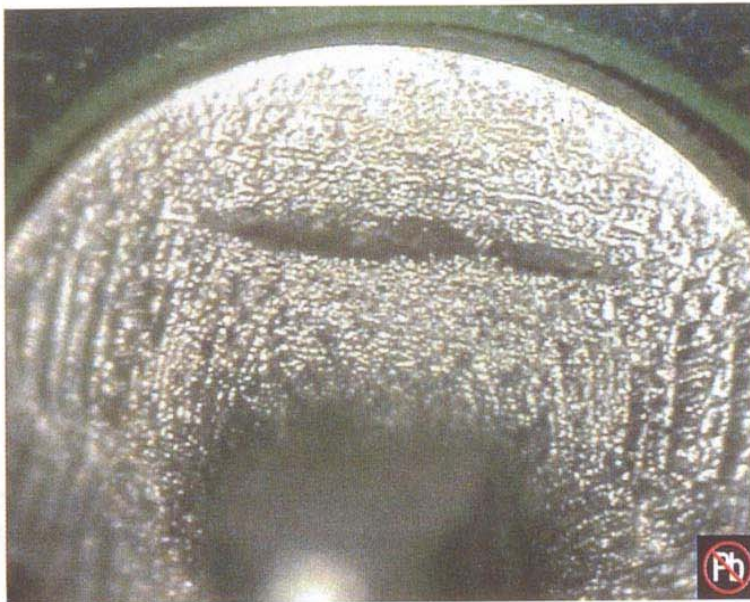


Figure 5-67

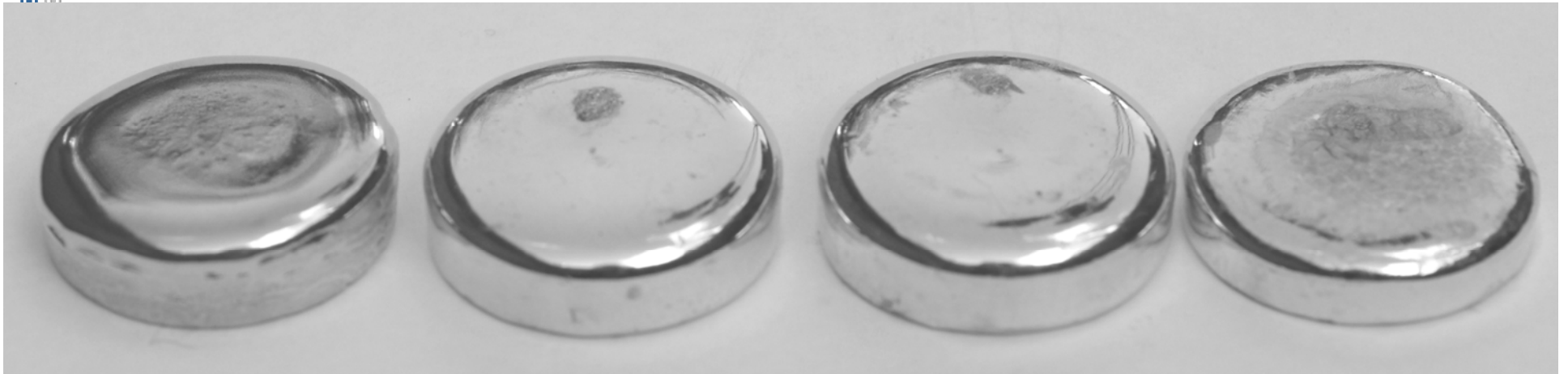
Acceptable - Class 1,2,3

- For connections made with lead free alloys:
 - The bottom of the tear is visible.
 - The tear or shrink hole does not contact the lead, land or barrel wall.

Defect - Class 1,2,3

- Shrink holes or hot tear in connections made with SnPb solder alloys:
- For connections made with lead free alloys:
 - The bottom of the shrink hole or hot tear is not visible.
 - The tear or shrink hole contacts the lead or land.

Not seen in SnCu based solders
such as K100, K100LD, SN100C



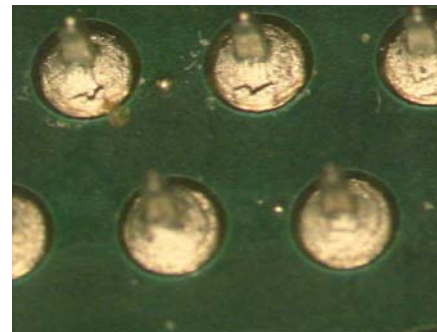
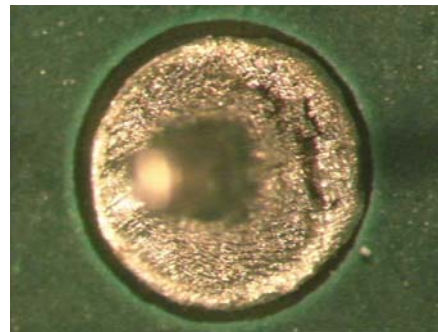
63/37

K100

K100LD

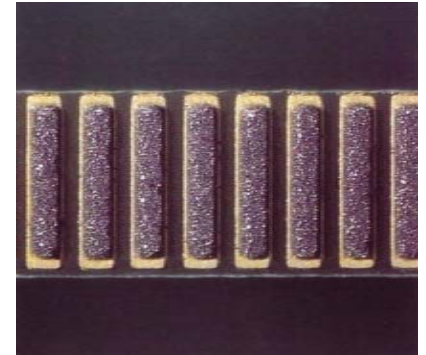
SAC

Solder Shrinkage SAC305



After 500 thermal cycles, iNemi Lead-free Wave Project 2006.

Lead-free SMT Assembly

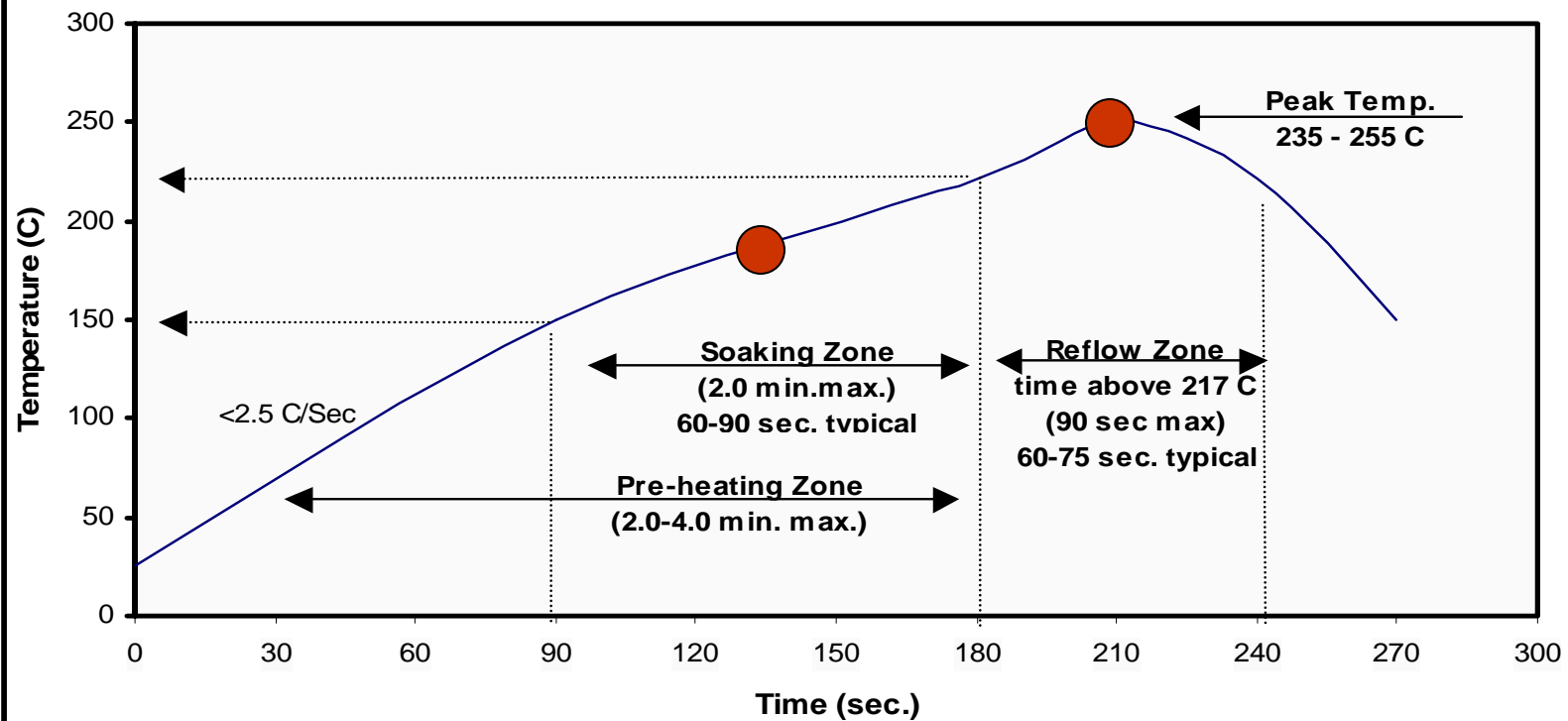


SMT Impact on Manufacturing

- Screen Printing and Paste Dispensing
 - Little change, rheological properties do not change, lower metal %
- Pick & Place Equipment
 - Little impact. Better placement accuracy may be needed due to less “self centering” of lead free alloys when molten
- AOI
 - Recalibration; joints are duller in appearance and less reflective
- Reflow
 - Significant impact due to higher melting alloy temperatures
 - Inspection, changes due to cosmetics and wetting characteristics
 - ICT changes due to no-clean flux residue hardening

Lead-free Reflow Profile

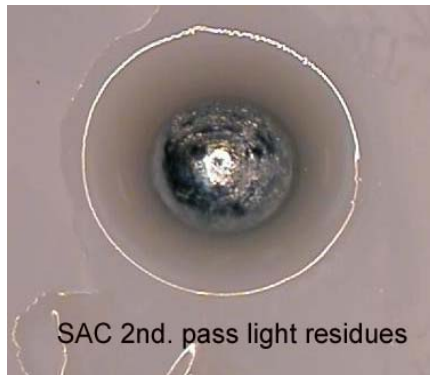
Typical profile for SAC in Air or N²



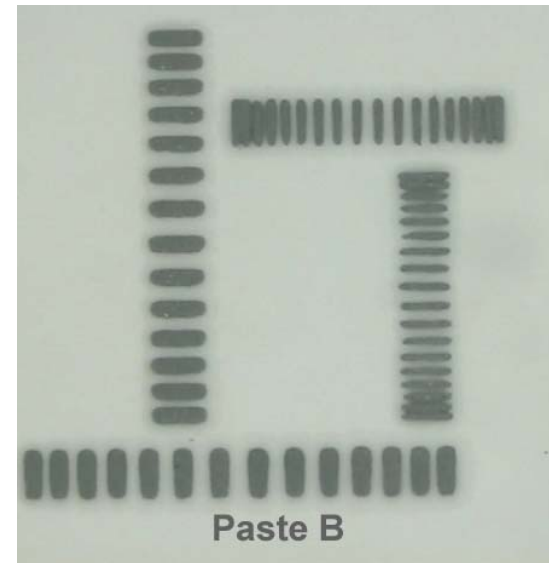
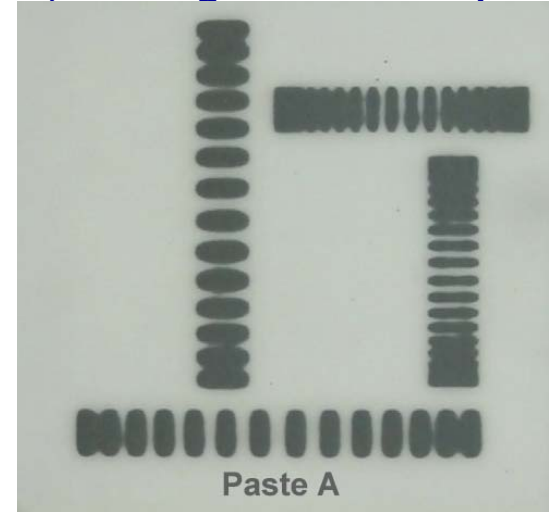
New LF Solder Paste Flux are Required

Below two lead-free SAC pastes heated to 180°C, showing different slump behaviors

- New activators
- New resins
- New gelling agents
- Better surfactants
- Oxidation inhibitors
- Alloy specific fluxes



Residue impacts ICT, cosmetics and cleaning and sometimes reliability



Solder Paste Qualification

Ask for more information

- Print speed
- Abandon time
- Stencil life
- Tack life
- **Solder ball potential**
- **Slump behavior**
- **Metallization Spread**
- **Reflow window**
- **Voiding potential**
- **Double reflow**
- **Cleanability, if W/S**
- **Pin testability, if N/C**



Little change

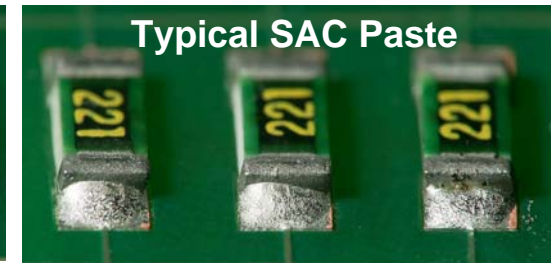


Change

Choose the right paste for the job



Kester EM907

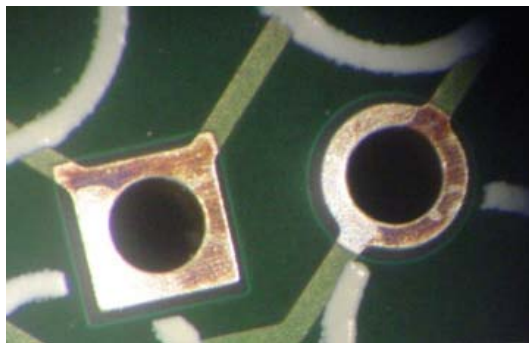


Typical SAC Paste

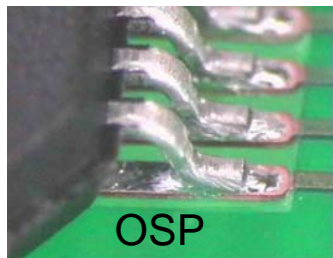
Same alloy, flux class, powder size but different finishes

The Impact of Board Finish

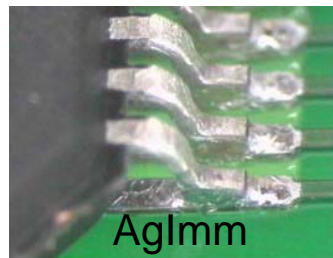
- Immersion Ag
- Immersion Sn
- ENIG
- Copper OSP
- HASL Lead-free
- Plated SnAg, SnCu



Silver Tarnish

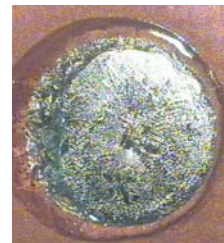


OSP



AgImm

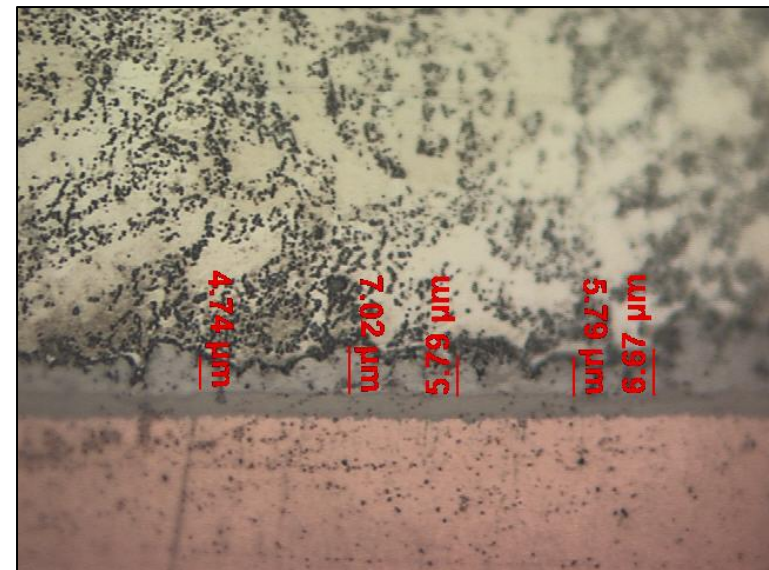
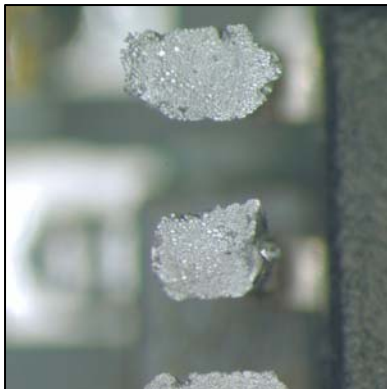
Copper Oxidation



	HASL	OSP	ENIG	Pd	Tin	Silver
Flat	no	√	√	√	√	√
Solderjoint	Cu-Sn	Cu-Sn	Ni-Sn	Ni-Sn	Cu-Sn	Cu-Sn
Contact	E-test, ICT	no	E-test, ICT, keypad	E-test, ICT, keypad	E-test	E-test, ICT, keypad
Wirebond	no	no	Al	Au, Al	no	Au, Al
Cost	\$	0.7 x \$	3 x \$	5 x \$	0.8 x \$	0.8 x \$
OEM's	all	all	most	few	30	150
Fab's	most	most	200	few	40	250
Reflows	6	2	6	6	2-3	6
Shelf-Life	18 mos.	6 mos.	24 mos.	24 mos.	6 mos.	12 mos.
Compliant Pin	+	-	-	-	++	+

Lead-free Profile Modification

- Longer TAL (Time Above Liquidus) results in improved wetting
- Higher peak temp equals improved wetting
- Wetting very much alloy and surface dependent
- Flux activity is a critical element
- Drawbacks of longer TAL
 - IMC growth
 - Residue effects
 - Joint cosmetics



Top, intermetallic bond thickening

Left, excessive preheat, deactivation

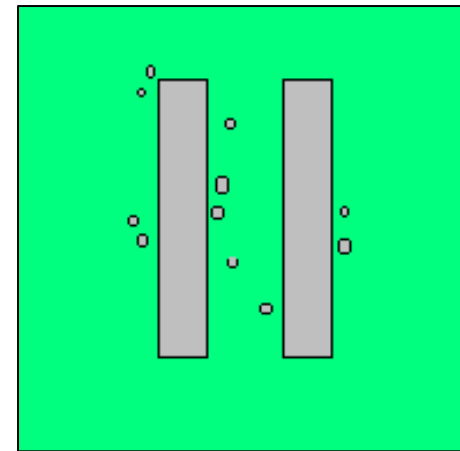
SMT Variables and Impact on Defects

- Components and board solderability
- Storage conditions and handling
- Stencil design
- Solder paste alloy/flux selected
- SMT environment
- Printer and settings
- Component placement
- Reflow equipment and profile
- Cleaner and cleaning solution if w/s
- Pin tester, pins and pressures

- Off-pad solderballing
- Mid-chip solderballing
- Tombstoning
- Bridging on fine-pitch
- Open joints
- Cold solder joints
- Voids

Solderballs

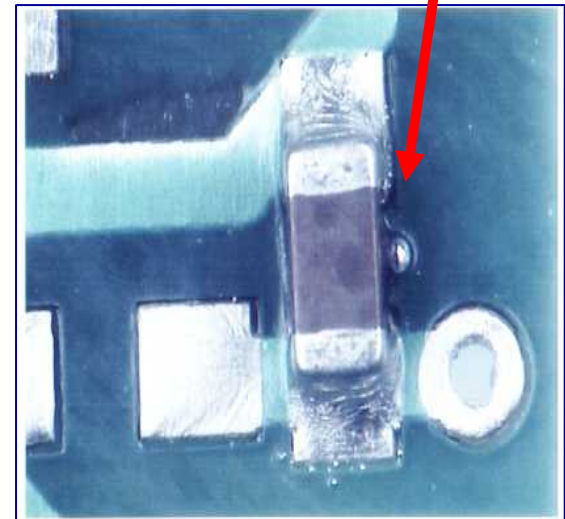
- **Away From Pad Area, Random Solder Balls:**
 - Moisture Absorption by Solder Paste. Commonly Caused by Refrigerated Paste Opened Prior to Returning to Ambient Temperature.
- **Around Pad Area:**
 - Paste Contains “Fines” (Extra Fine Powder), Carried Away by Flux During Heating.
 - Hot Slump Behavior
 - Excessive Preheating; Flux deactivation
- **Oxidized Solder Powder, Flux Medium Too Weak to Remove Oxide Layers, Poor Hot Slump.**
- **Printing Defects:**
 - Paste Buildup on Underside of Stencil.
 - Excess Paste Deposit.
 - Poor gasketing of Stencil.
 - Excessive Squeegee Pressure.



Solder Beading

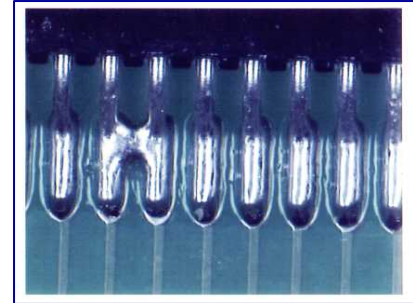
- Excess Solder Paste Slump During Preheat Stage
- Metal Loading Percentage of Paste Too Low
- Preheat Temperature Too High or Too Long
- Paste Deposition Excessive
- Stencil Aperture to Pad Ratio
- Component placement pressure

Mid-chip Balling



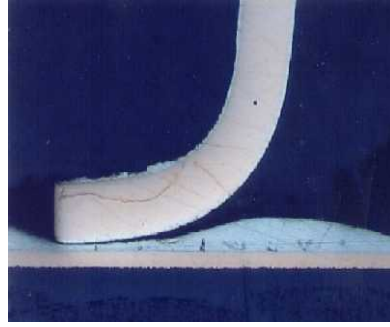
Bridging

- Excessive solder paste slump.
- Solder paste deposition excessive.
- Poor resolution of paste deposit.
- Paste smearing on bottom side of stencil.
- Component placement pressure too high.



**Bridging of
two chip
capacitors**

Non-Wetting



- **Poor solderability of pads or component termination, oxidation**
- **Contamination of pads or component termination**
- **Preheat time/temperature too long, deactivation of flux medium**
- **Flux activity insufficient**

De-wetting

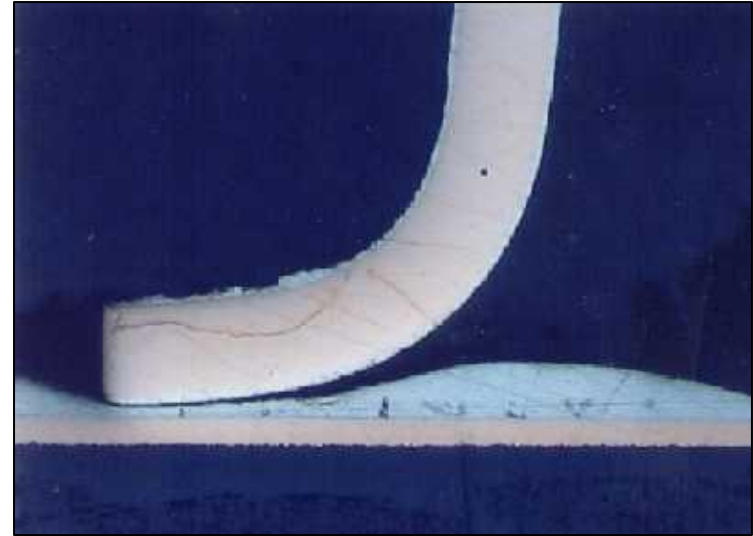
- Base metal difficult to solder
- Solderable coating too thin
- Base metal contamination
- Improper treatment of base metal prior to plating or tinning process.
- Time above liquidus too long or too high peak temperature



Tombstoning Solutions

- Adjust placement machine (offset)
- Increase pre-heat soak
- Insure uniformity of solderability
- Less active flux medium
- Increase placement down force
- Insure adequate paste volume
- Use alloy with slight pasty range

Open Joints



Causes

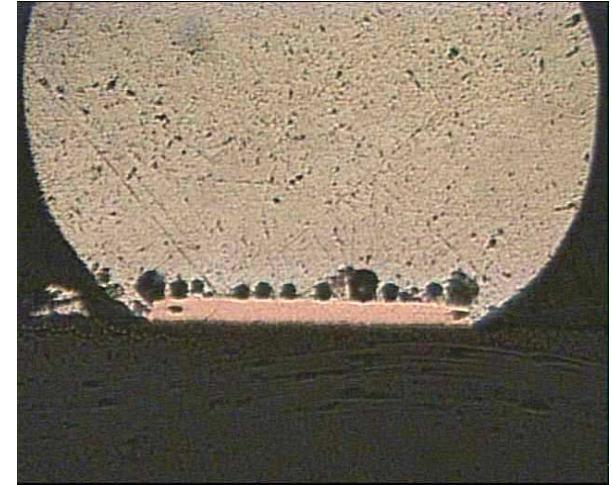
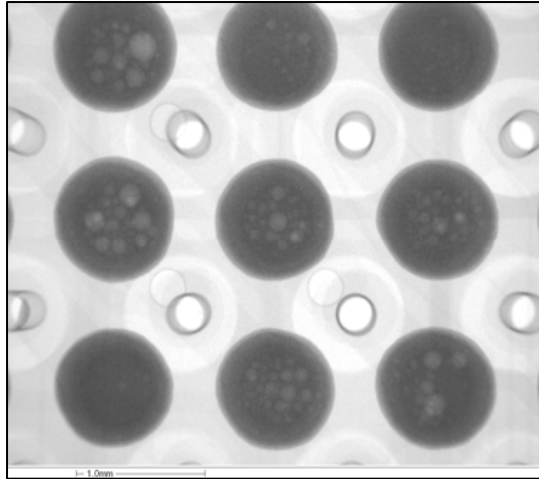
- Damaged component leads
- Poor solderability
- Insufficient flux activity
- Flux thermal stability

Solutions

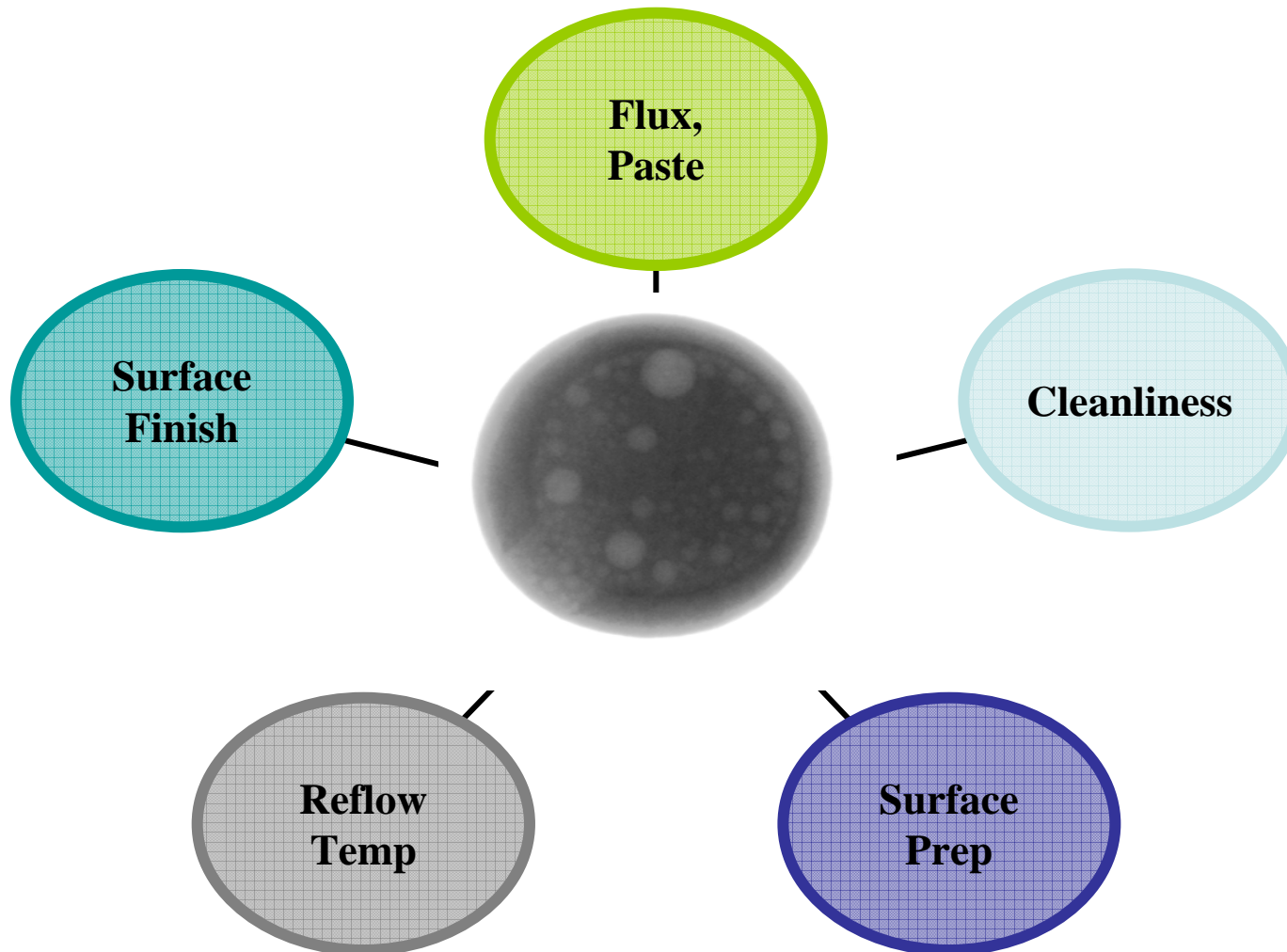
- Better handling/placement
- Reduce pre-heat input
- More active or higher solids content medium

Voiding Causes

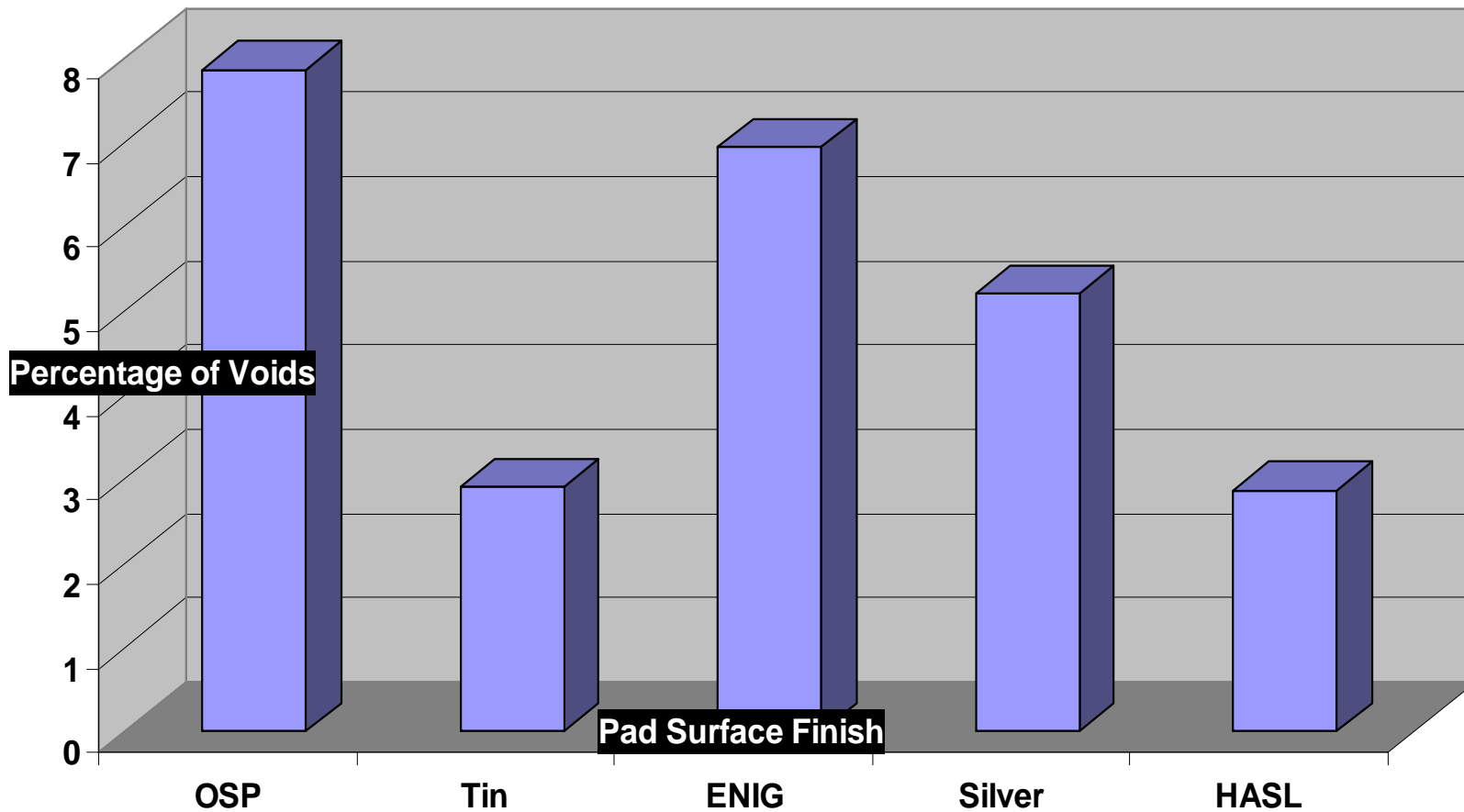
- Alloy flow rate
- Metallization
- Incorrect profile; more soak time required
- Insufficient time above liquidus temperature
- Flux chemistry, resin and solvent choices
- Component design, entrapment of flux by-products
- Plating chemistry, organic content, plating thickness



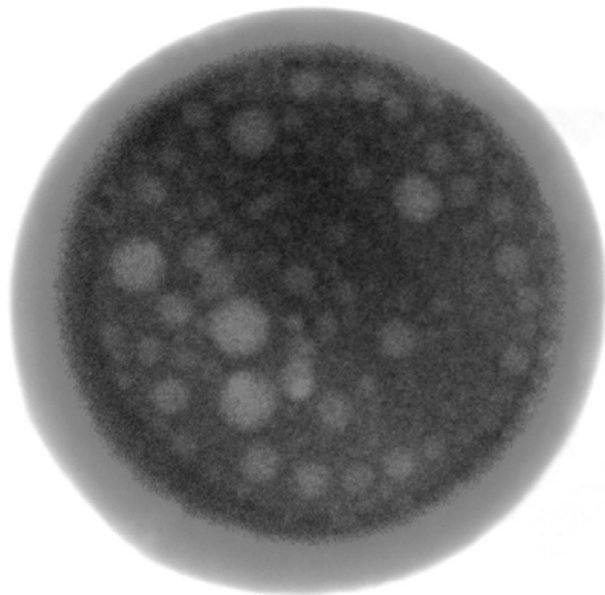
Conspiracy of factors and many causes



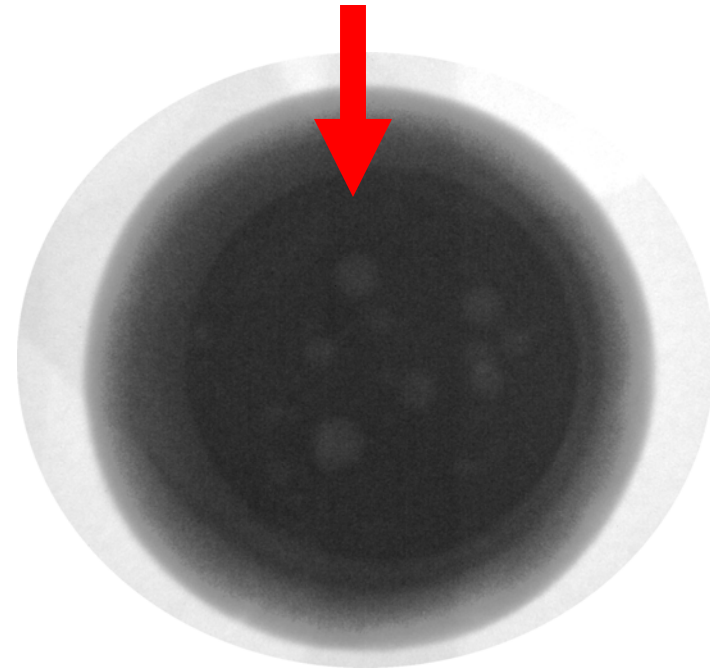
Dage, SMTA Int'l 2004



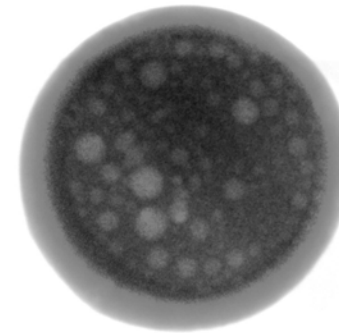
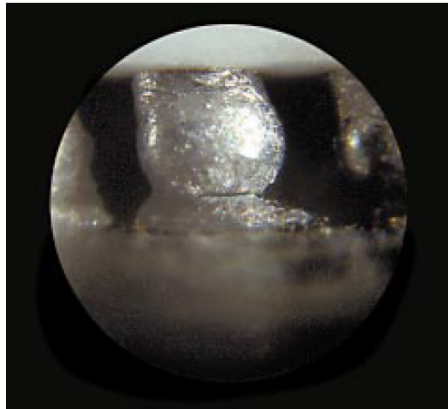
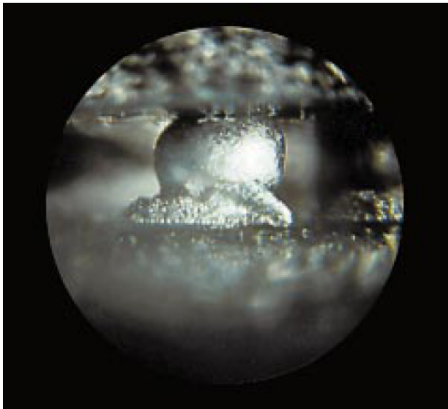
Assembly Confirmation modified plating chemistry for Ag Imm



**Silver Immersion
New Process Spec.**



IPC-610D, BGA assembly with lead-free solders



Acceptable - Class 1,2,3

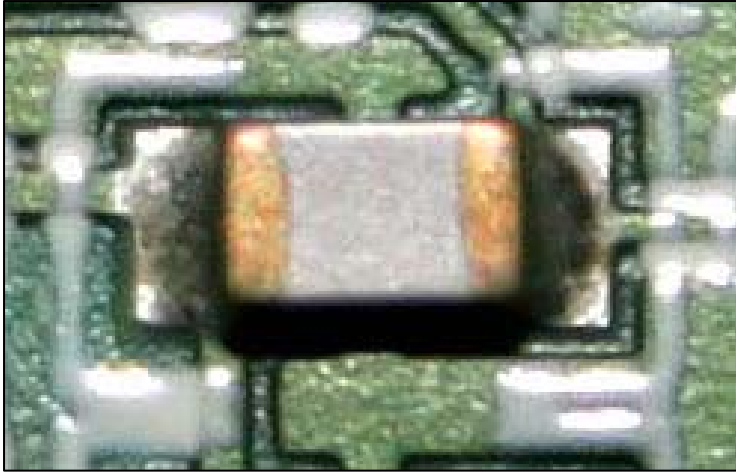
- 25% or less voiding of the ball x-ray image area.

Defect - Class 1,2,3

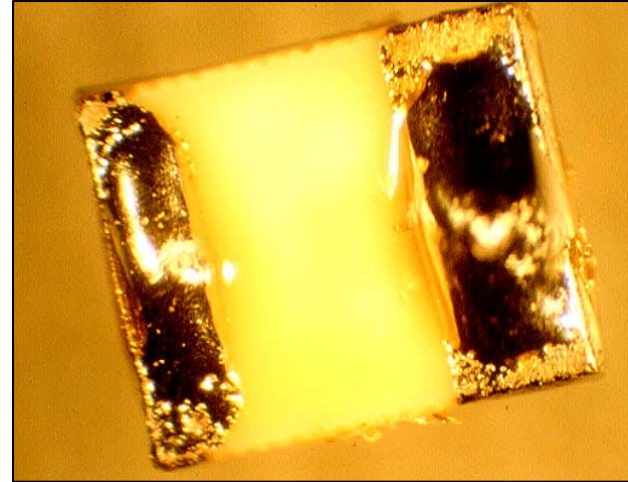
- More than 25% voiding in the ball x-ray image area.

- ☐ Biggest problem area with lead-free solders
- ☐ Insufficient wetting or ball collapse issues
- ☐ Thermal profile is critical, verify temperature at ball site
- ☐ Voids and micro-voids issues
- ☐ X-ray and endoscopic examination recommended

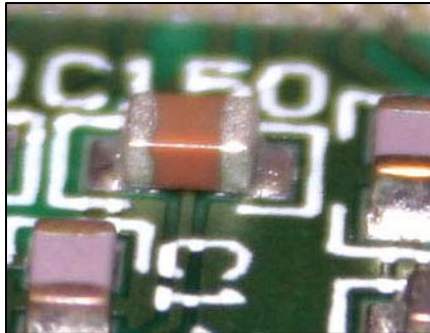
Termination Issues



Discoloration of terminals SAC305



Leaching of base metals



No discoloration with 63/37

- ☐ Excessive peak and time above liquidus
- ☐ Parts incompatibility to a lead-free process
- ☐ Metallization impurities, discoloration only

ENIG Discoloration, Profile Related



**First SMT Assembly with SAC305 profile and then waved with SAC305,
Cleaned in straight DI water 120°F**

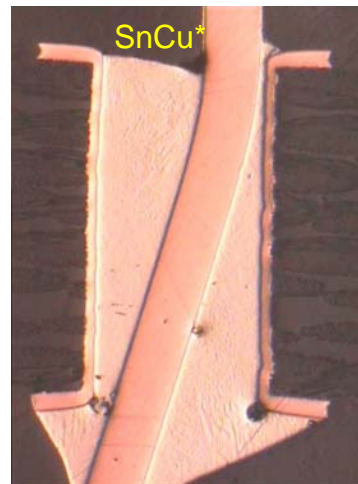
- ☐ Water contamination, flux reactions
- ☐ Gold thickness
- ☐ Excessive temperatures in reflow
- ☐ Gold, plating impurities



Lead-free Wave Soldering

Wave Soldering – Solder Behaviors

	SnPb	SAC	SnCu based
Wetting Speed	Fast	Medium	Slow
Contact Time	Shortest	Longer	Longest
Pot Temperature	465-510 °F	500-525 °F	510-535 °F
*Dross Formation	1x	1.8x	2x



Similar wetting with modifications to the process

Note: SnCu with additives used

Solder Properties - Most Popular Alloys

	K100LD	SnCu*	SAC305
Melt Point	~227C	~227C	217-220C
Pasty Range	0	0	3C
Appearance	Shiny	Shiny	Dull
Shrink Holes	No	No	Yes
Copper Dissolution (Sn63 = 1)	0.8	1.0	2.1
Pot Management	Easiest	Easy	Difficult
Reactivity to Equipment	Low	Low	High
Suggested Pot Temperature	255 – 265°C	255 – 265 °C	250 – 260 °C
Approximate Relative Cost (Sn63 = 1)	1.5	1.5	3.0

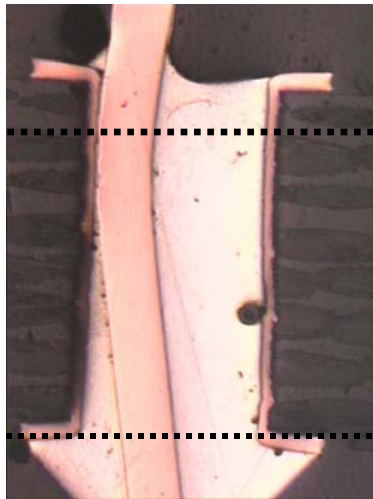
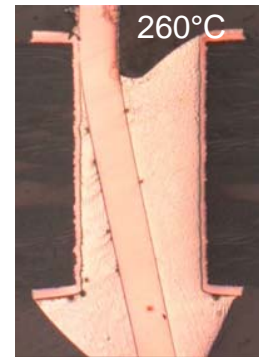
* With minor additives

Lead-free Liquid Flux Compatibility

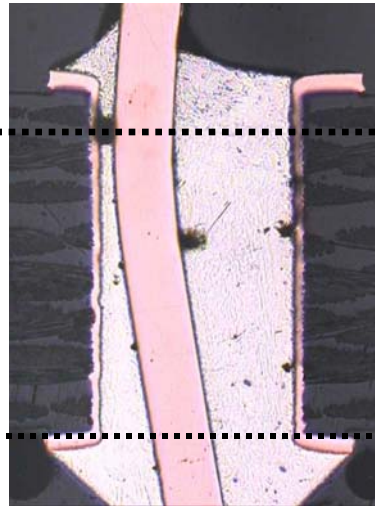
	VOC-Free (water is solvent)	Alcohol-based
No-Clean, Low Solids, No Rosin	Best for LF *	Not suitable for LF
No-Clean, Low Solids, With Rosin	N/A	Suitable for LF
Organic Acid (Water washable residues)	Best for LF *	Suitable for LF
Rosin-based	N/A	Suitable for LF

* Best selections for lead-free wave soldering

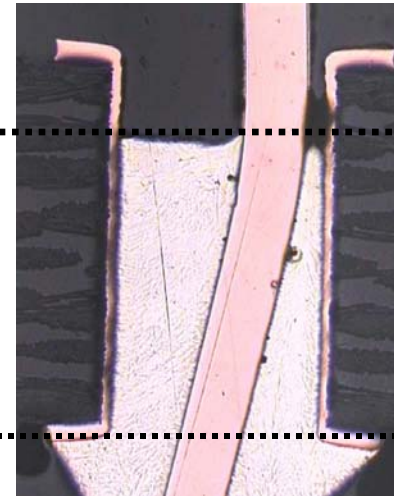
Impact Solder Pot Temperature and Finish



Ni/Au



Ag Immersion



Copper OSP

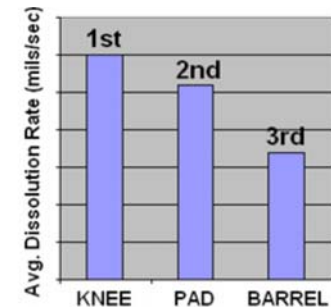
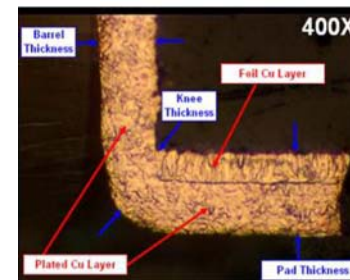
**75 %
Vertical
Hole fill**

Pure tin leads, SAC at 250°C, 1 Meter/minute, ROL1 Flux

K100LD has the Lowest Copper Dissolution

- Minimizing Copper Dissolution is critical with the conversion to lead-free soldering.
- Lead-free alloys dissolve Copper and other metals faster than leaded solder.

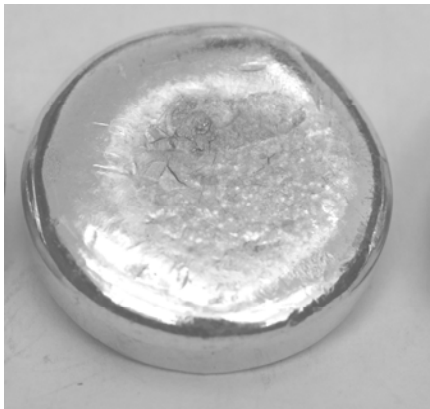
Alloy	Relative Rate of Copper Dissolution
K100LD	0.8
Sn63	1.0
SnCu+Ni	1.0
SAC+Bi	1.6
SAC305	2.1
SnCu	2.2
SnAg	2.3
Pure Tin	2.4



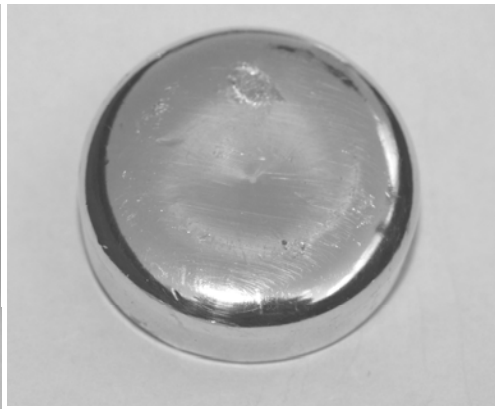
Dissolution of lead with SAC solder

Dullness

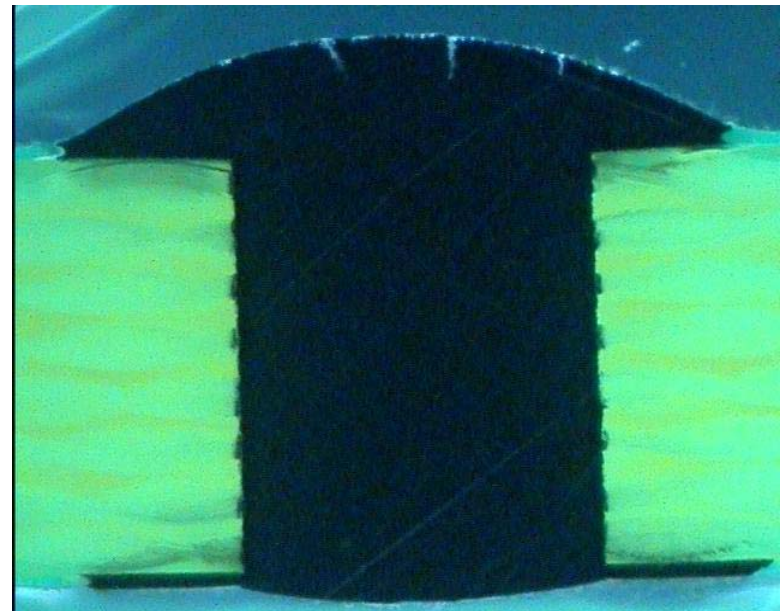
- Many lead-free alloys produce matte-finish, dull solder joints
- This dullness comes from a small amount of surface shrinkage when the alloy cools.
- This surface shrinkage (also known as “hot tears” or “shrink holes”) can result in cracking that goes somewhat beyond the surface



SAC305



K100LD

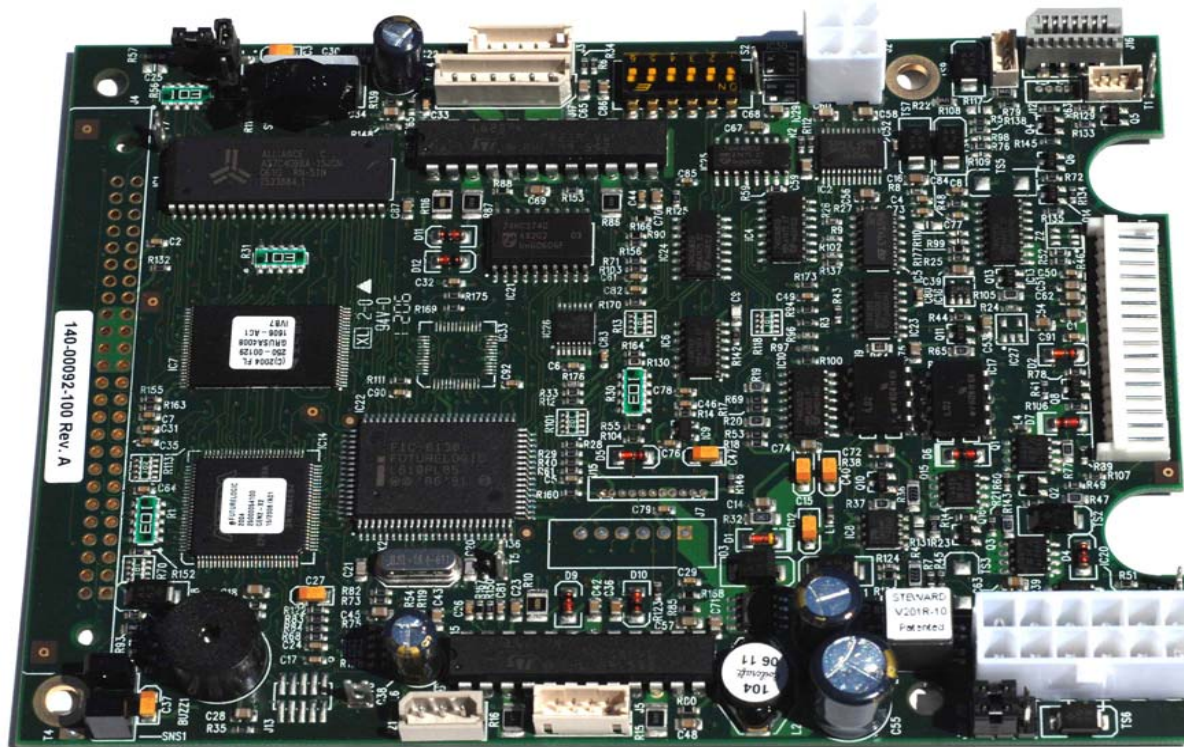


SAC305 Shrinkage Cross-section

SMT Dynamics, Anaheim CA

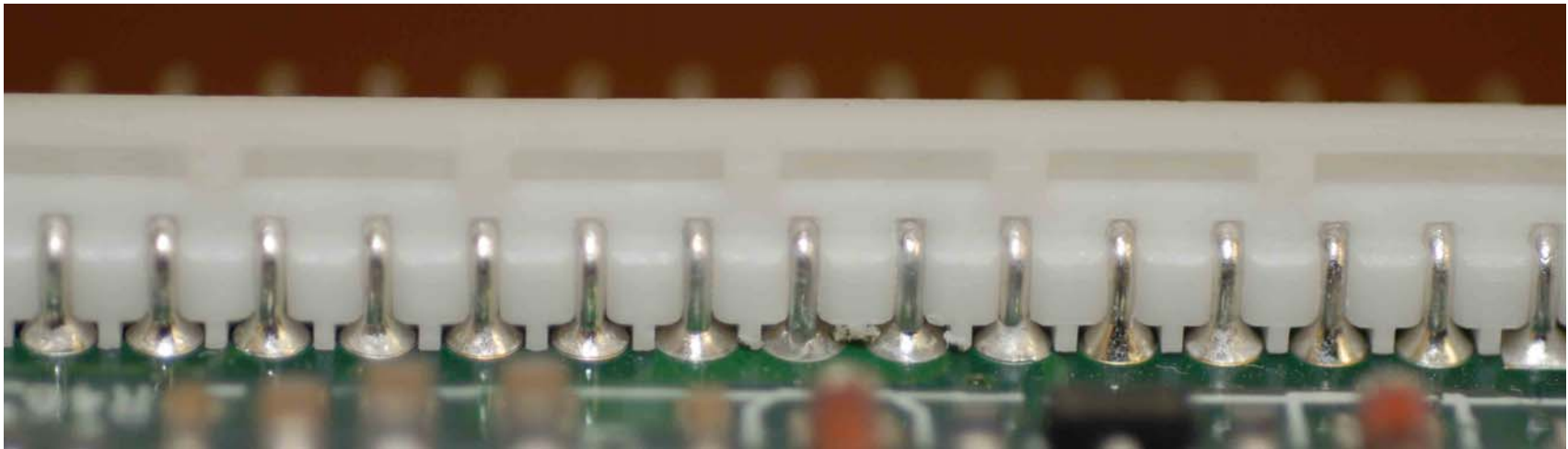
SnCu (K100) with 2235 Flux; SAC305

R520A and K100, 331 Flux 66 core wire



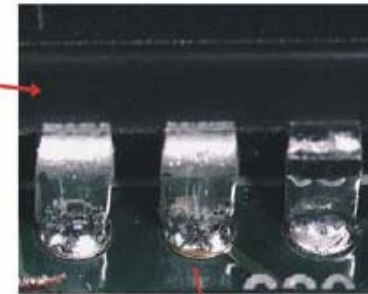
FutureLogic Thermal Printer ENIG Board 300,000+ assembled

K100 Wave Soldered Connector 0.063" thick ENIG PCB

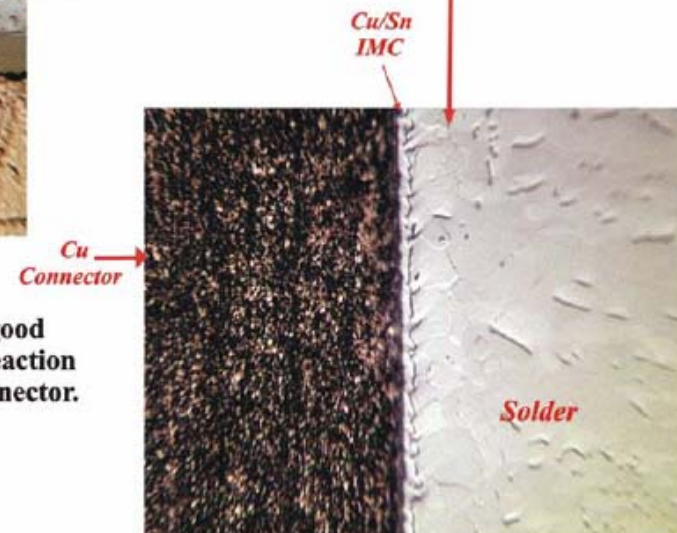
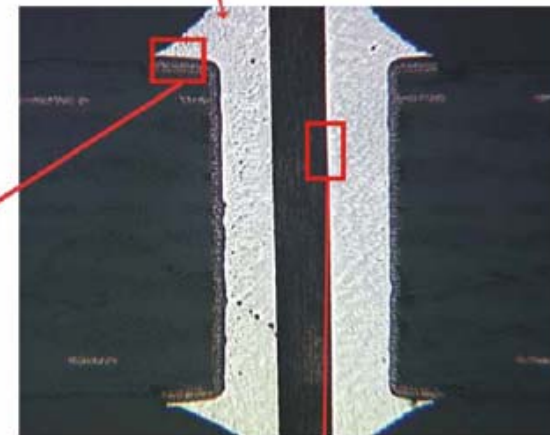
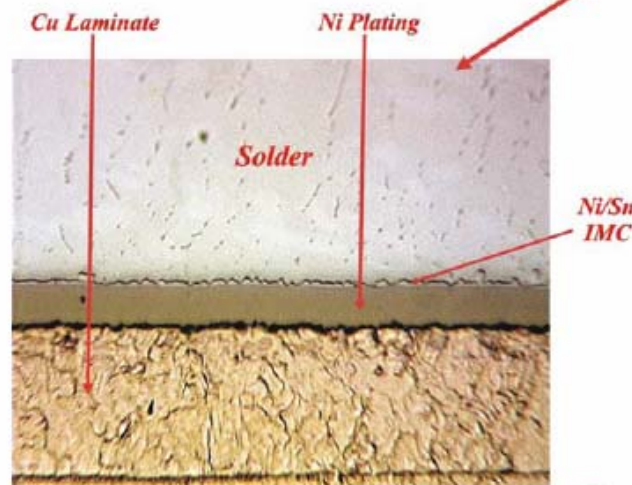


FutureLogic Board

Tests Done
X-Ray
Cross-sections
IPC 610 Inspection



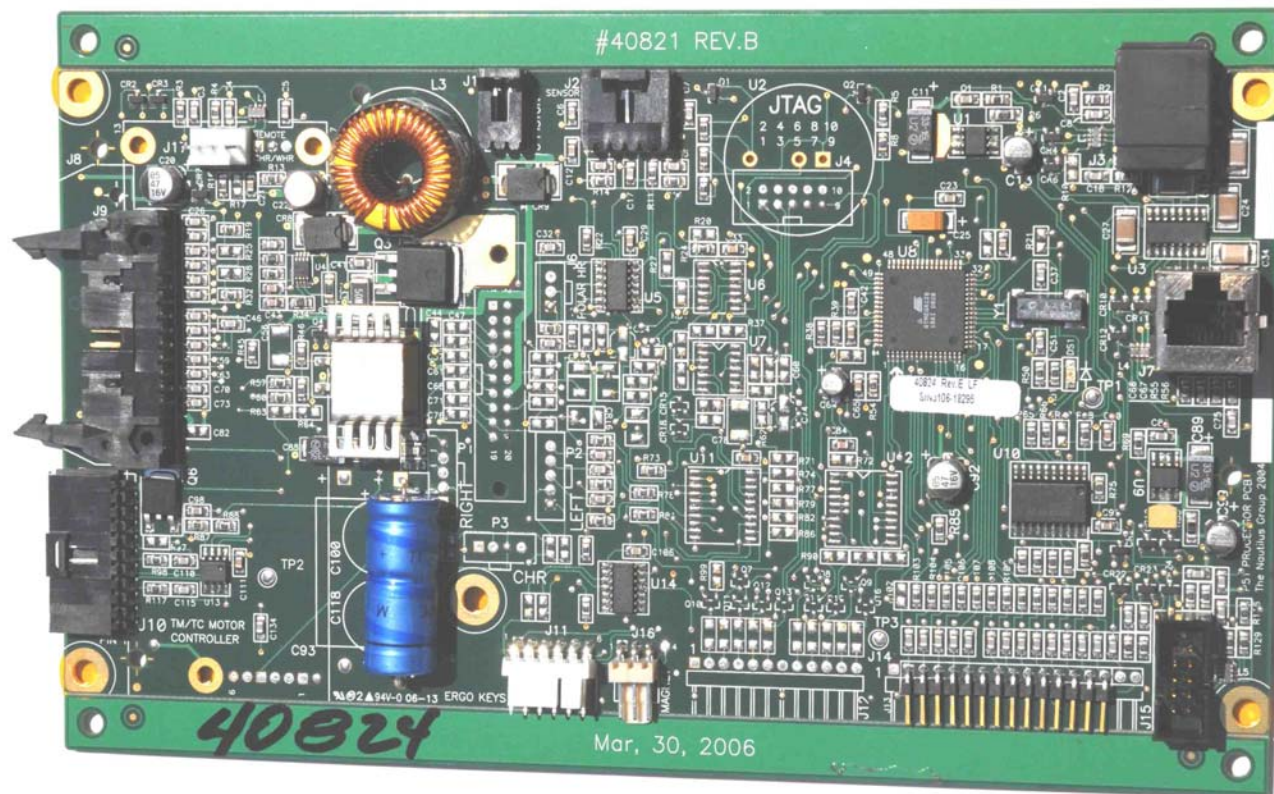
The photomicrograph (below) reveals an adequate Ni/Sn intermetallic compound (IMC) reaction layer between the solder and the Ni barrier plating on the Through-hole walls.



The photomicrograph (right) reveals a good Cu/Sn intermetallic compound (IMC) reaction layer between the solder and the Cu connector.

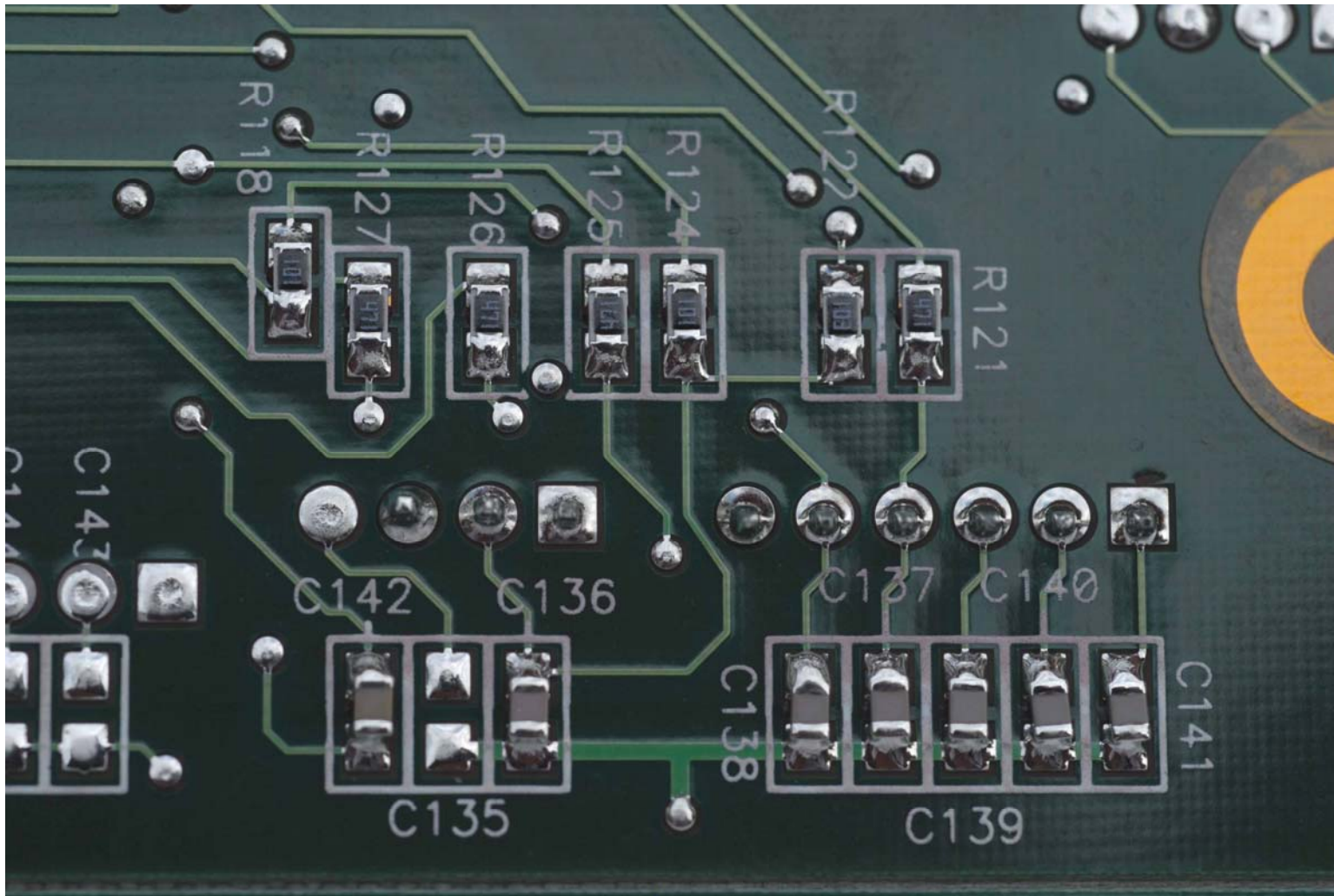
Ayrshire Electronics LF Implementation

- They built 3 board types for Nautilus Europe with Kester K100LD bar, 2235 flux and SAC305 EM907



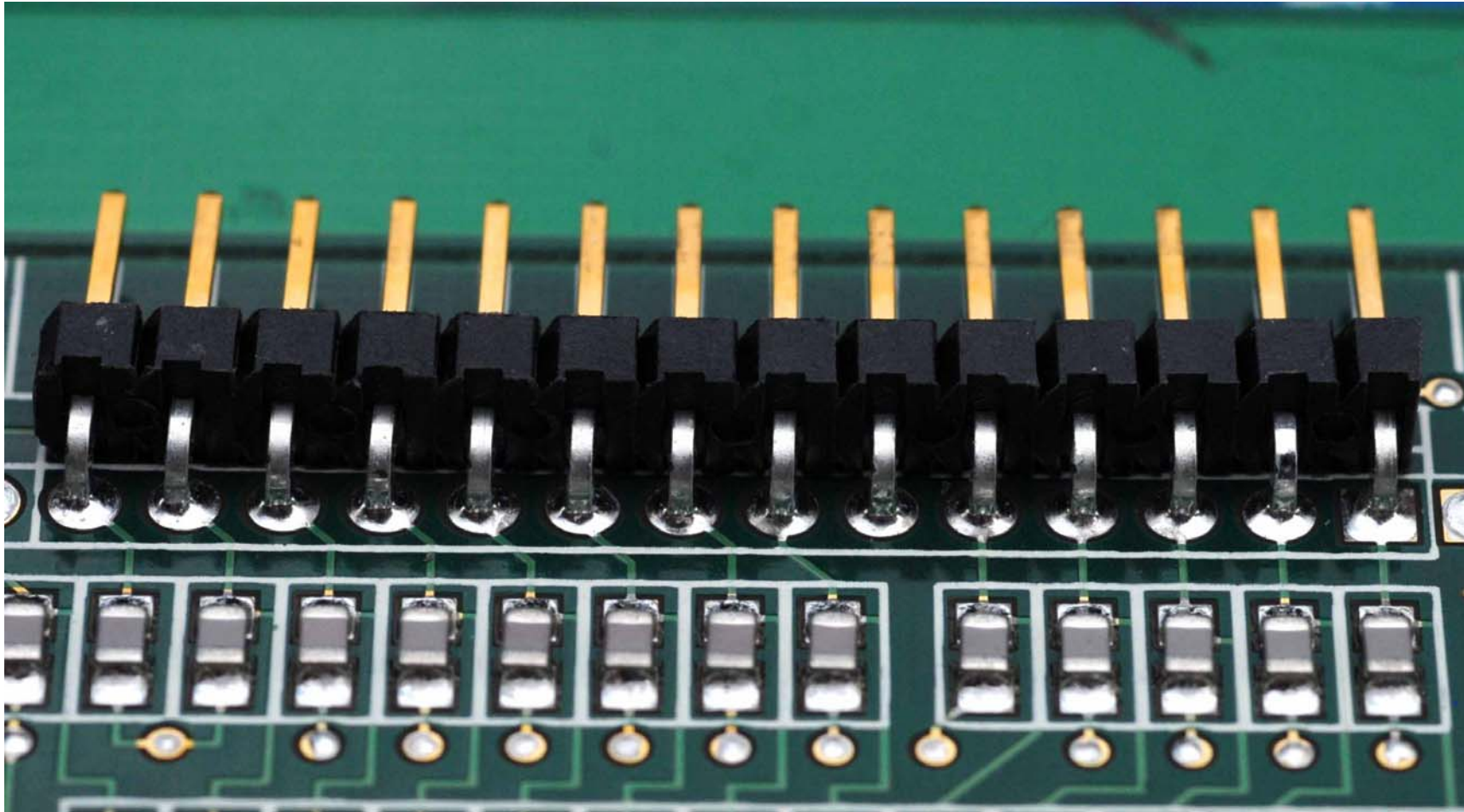
Mixed technology board with top and bottom-side SMDs, 0.063" SN100CL

Bottom-side SMDs and PTHs done with K100LD and Kester 2235



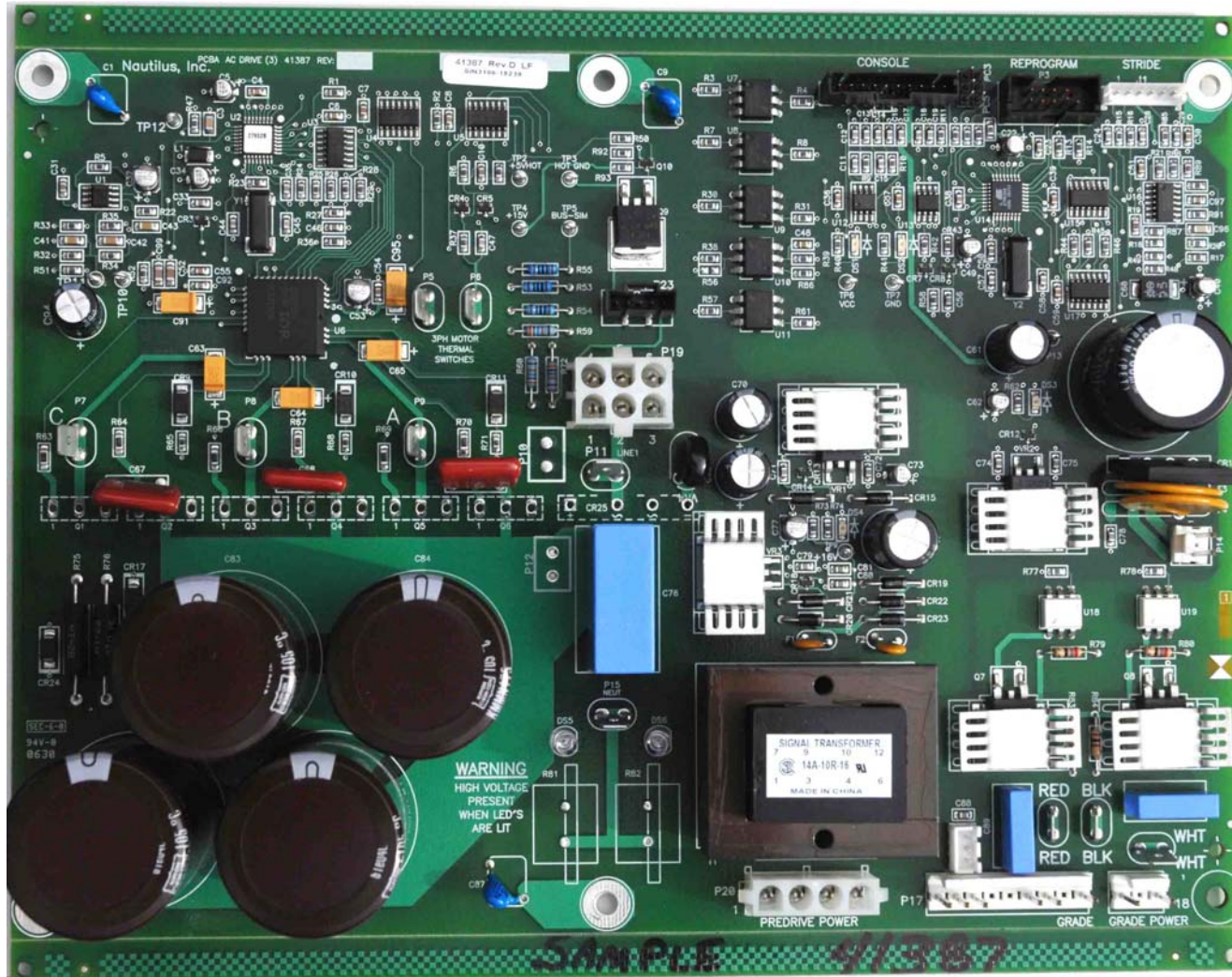
The boards exhibited no defects and bright joints

K100LD Excellent Top-side Fillets; No Dullness, No Shrinkage

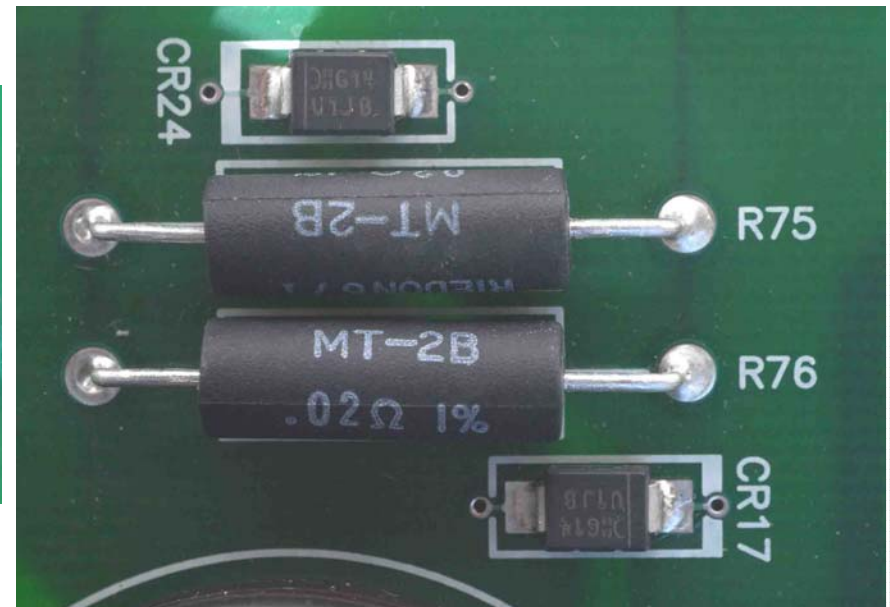
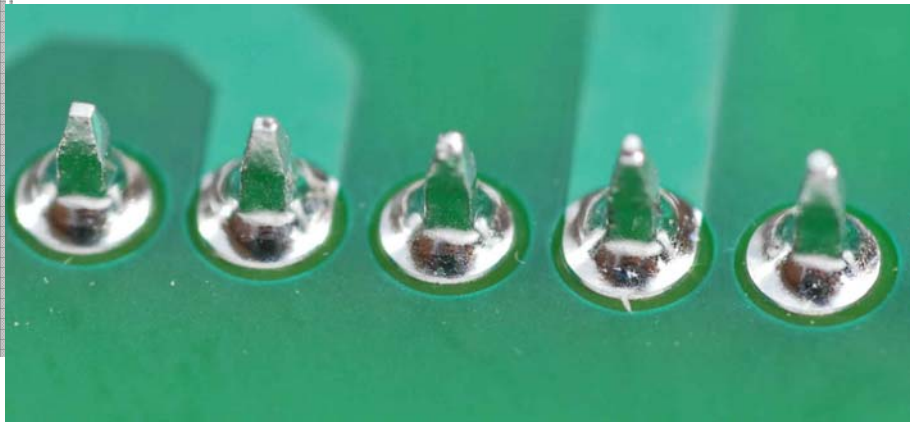


SAC305 EM907 was used for top-side SMDs

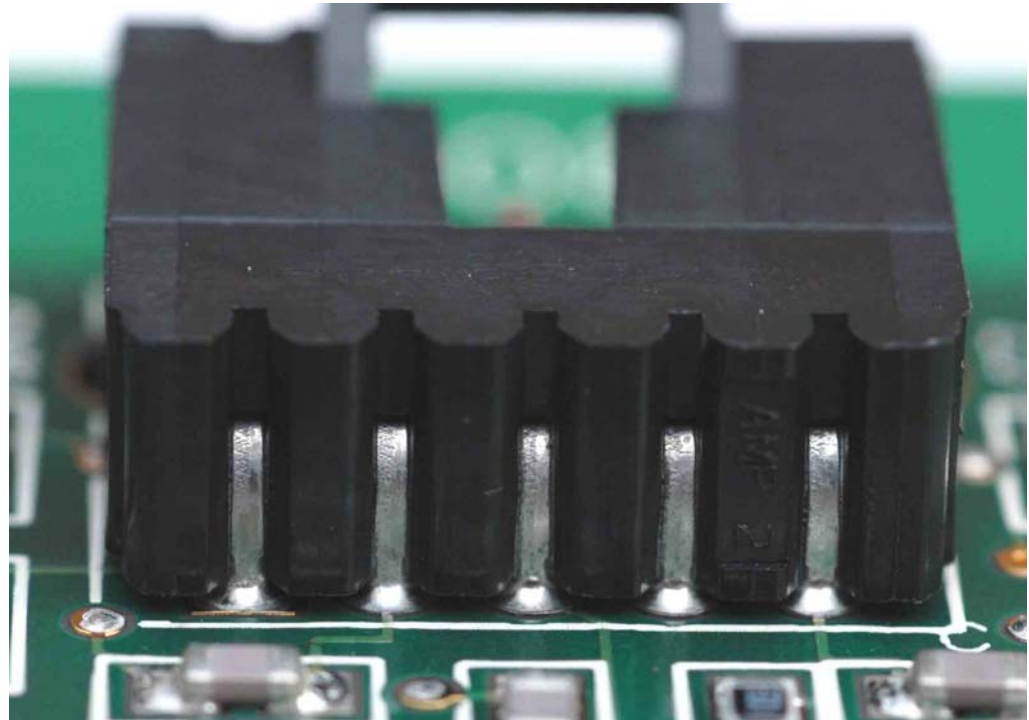
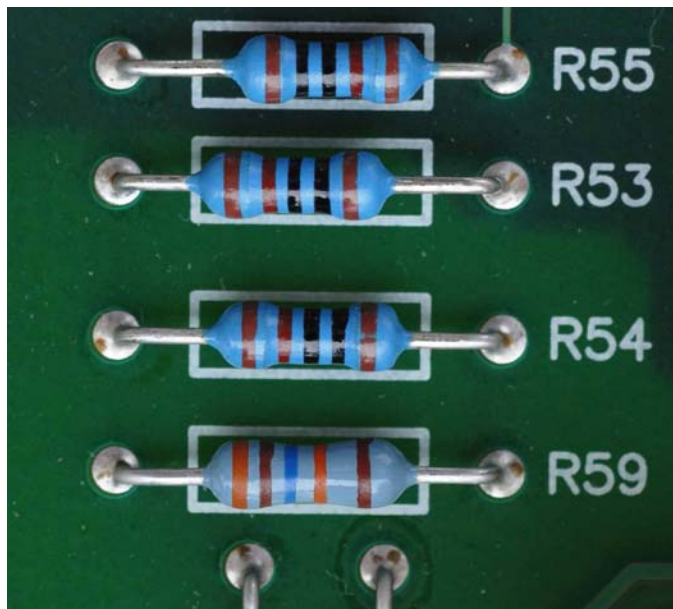
K100 and 2235 Flux with SAC305 EM907 Top-side reflow, **0.093"** Thick SN100CL Finished



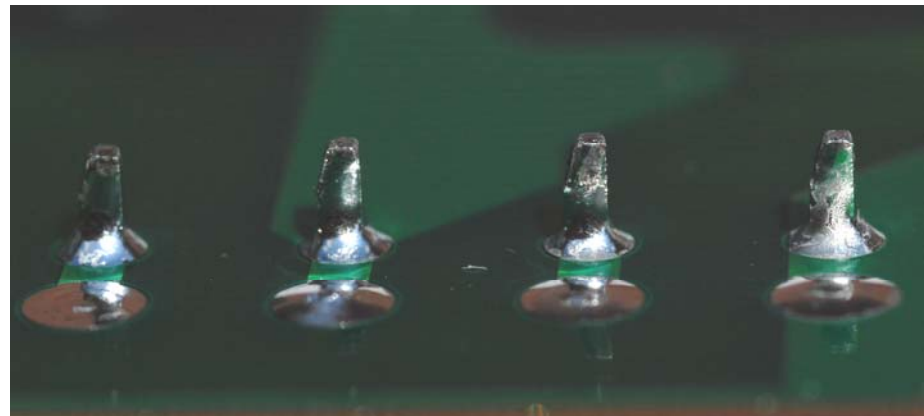
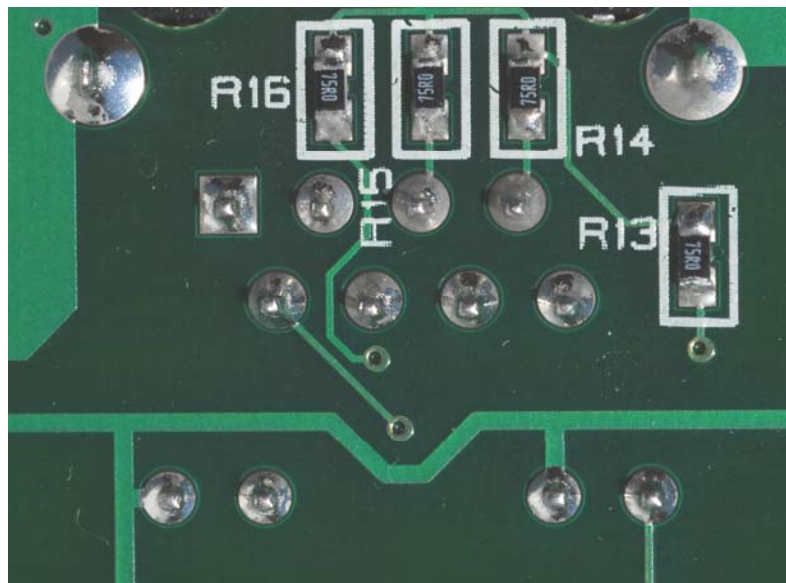
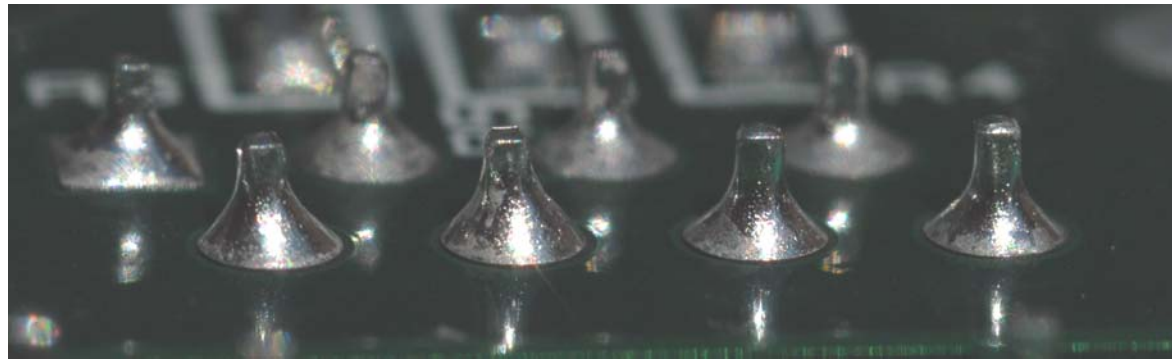
K100LD excellent defect-free bottom-side and top hole-fill



K100LD on 0.093" thick board with excellent hole-fill



SnCuNi +Bi (K100LD) Joints



Optimized Wave Soldering Process for SnCu Enhanced Solders

- Wave pot temp. 260-265°C
- Conveyor speed 3.0-3.5 feet per minute
- Contact time 3-5 seconds
- Contact width 2 inches approx.
- Board to wave contact thickness $\frac{1}{2}$ to $\frac{3}{4}$
- Board preheat 100 to 130 °C, flux dependant
- Flux was either sprayed or foamed

Wave Defects - Cause and Effects

- Solderability of boards and components
- Lead-free solder alloy selected
- Flux selection
- Flux application and control
- Equipment process conditions
- Board & component design
- Solder mask type
- Cleaning process compatibility
- Conformal coating and flux compatibility

- **Non-wetting, skips**
- **Poor hole filling**
- **Bridging**
- **Fillet Lifting**
- **Solder balls**
- **Voids**
- **De-wetting**
- **Mask blistering**

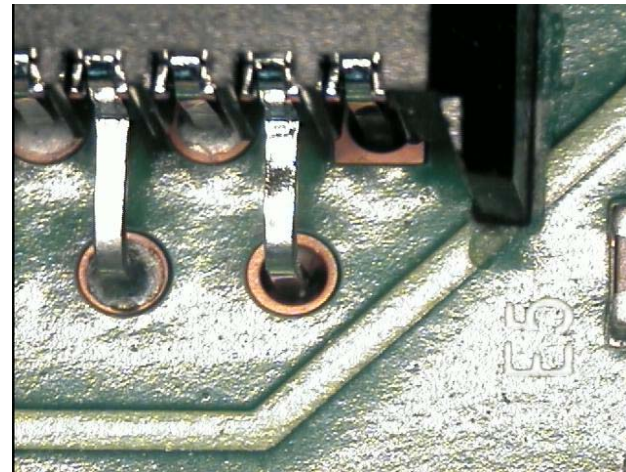
Skips, Non-Wetting, Poor-Hole Fill and De-Wetting

No wetting; skips

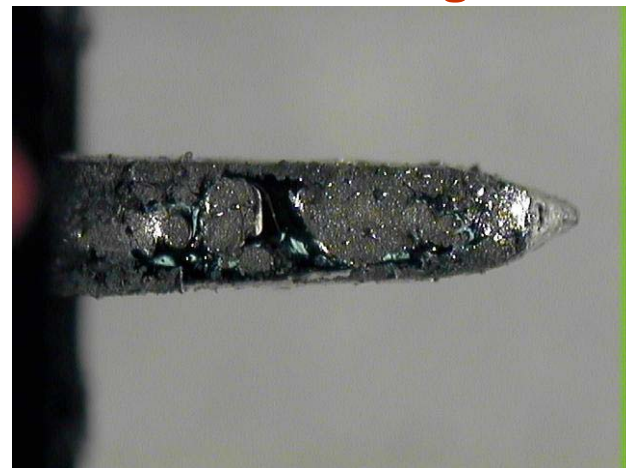
- Insufficient flux
- Lack of flux activity
- Solder wave low or uneven
- Conveyor too fast
- Board warp
- Lead-to-hole ratio too large
- Soldermask in hole
- Shadowing
- Pump too slow

De-wetting

- LF alloy dependent
- Pot temperature
- Contact time



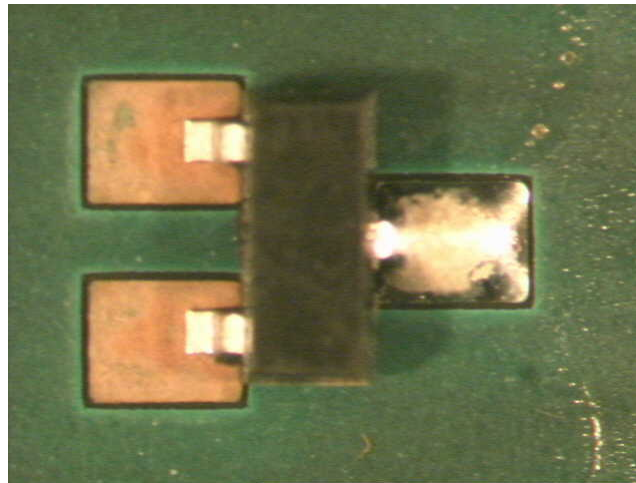
Non-wetting



De-wetting

Shadowing Effects

Surface tension differences

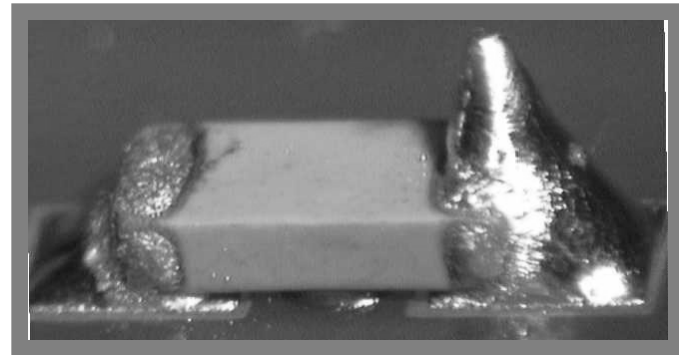


SAC305 using no-clean flux, board OSP

- ☐ Increases due to higher surface tension of lead-free solders
- ☐ Design issue
- ☐ Wave parameters, such as use of chip wave or higher impeller speeds

Icicles or Flagging

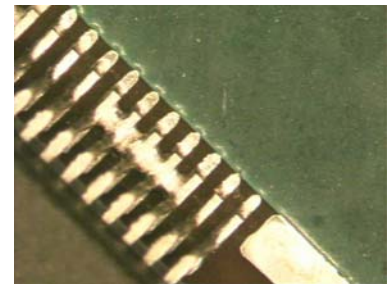
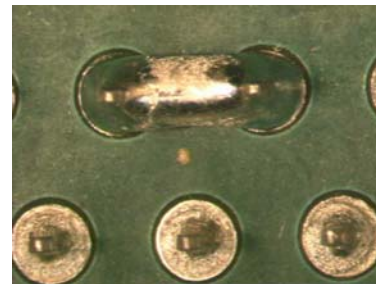
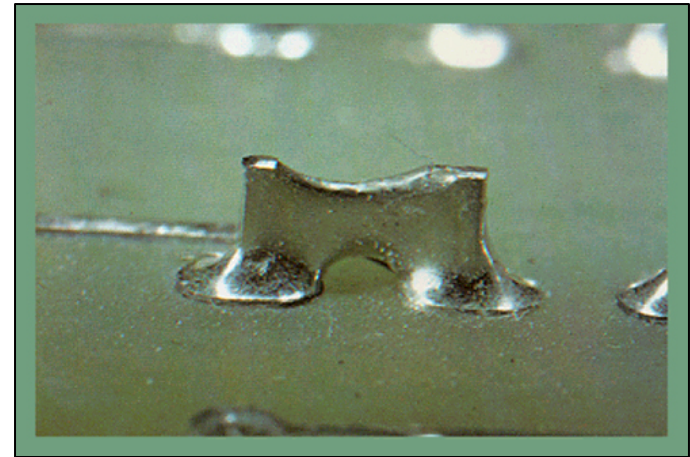
- Solder temperature low
- Solder contamination
- Preheat too low/high
- Solder wave height low
- Preheat temperature low
- Conveyor speed high
- Conveyor angle low
- Contact time
- Insufficient flux



Fluxes for lead-free soldering with sustained activity reduces icicling.
Higher solids percent and/or a higher acid number also helps.

Bridging

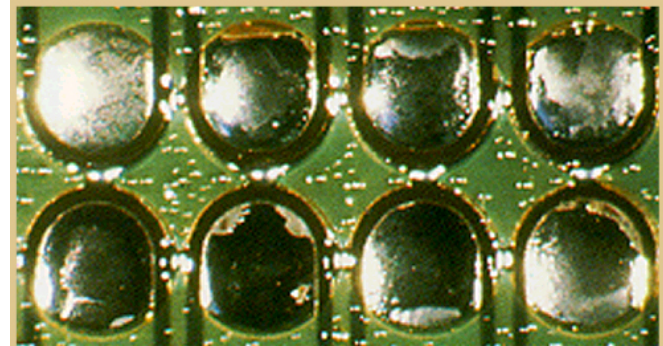
- Solder temperature low
- Insufficient flux
- Preheat too low/high
- Flux not active enough
- Flux over thinned or old
- Leads too long
- Component/board design
- Orientation to wave
- Conveyor speed too slow/fast
- Contact time



**Lead-free alloys wet surfaces at a slower rate and have slower peel back.
Good sustained activity in the flux is needed.**

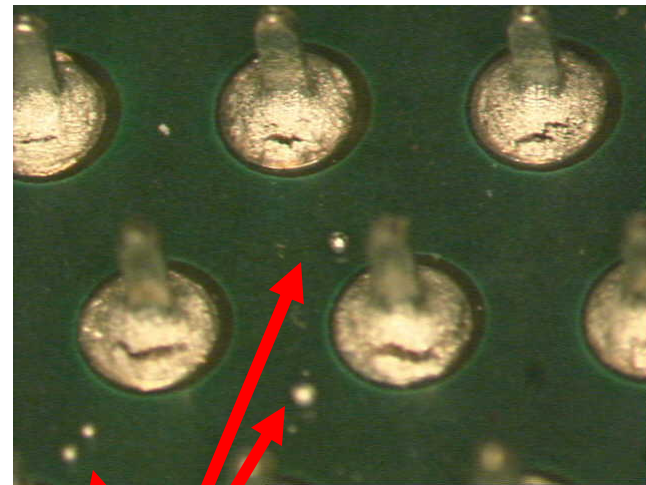
Solder Balls

- Under-cured solder mask
- Solder temperature too high
- Insufficient flux
- Flux not evaporated before wave
- Incompatible flux and mask
- Correct flux for application
- Contact time



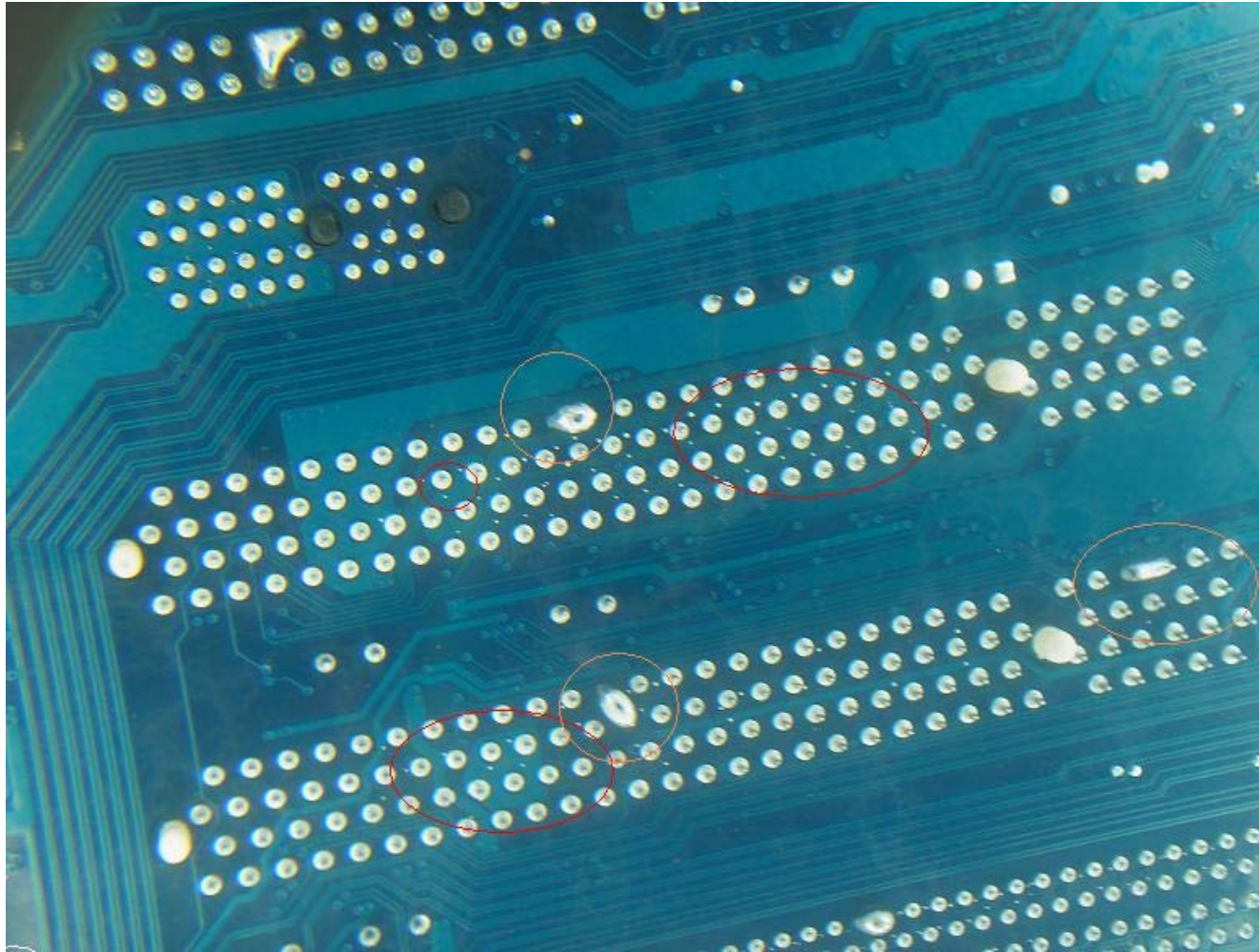
SAC305 Solder Balls, No-clean flux

- Flux can be cause
- Solder temperature
- Solder mask cure
- Contact time or dwell



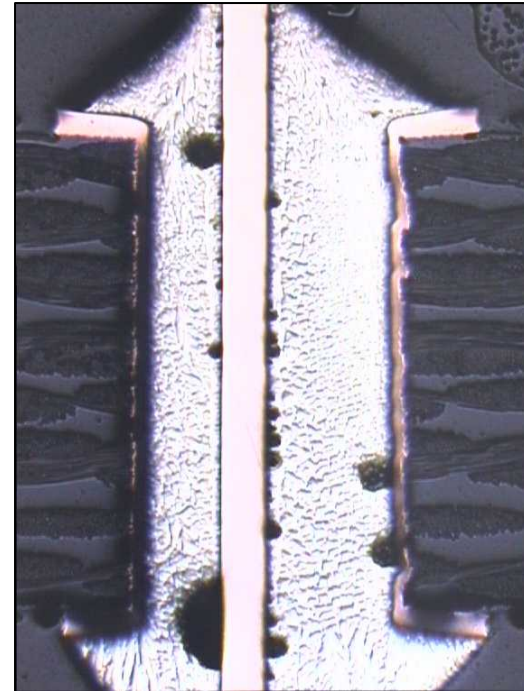
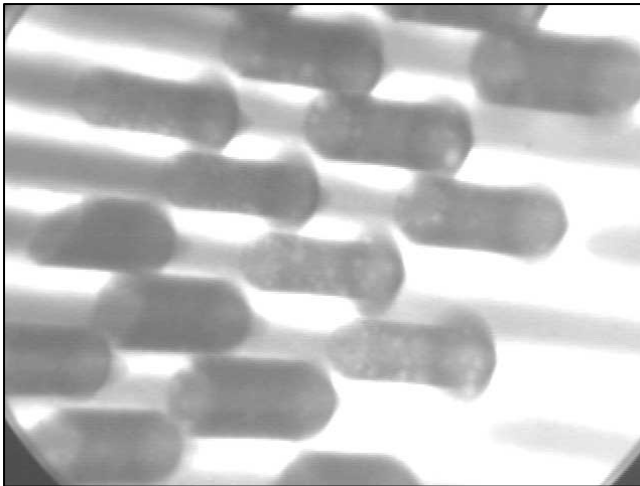
Solder balls adhering to mask

Solder Balls using SAC305 and VOC-Free No-clean Flux



Voids in Wave Soldering with Lead-Free alloys

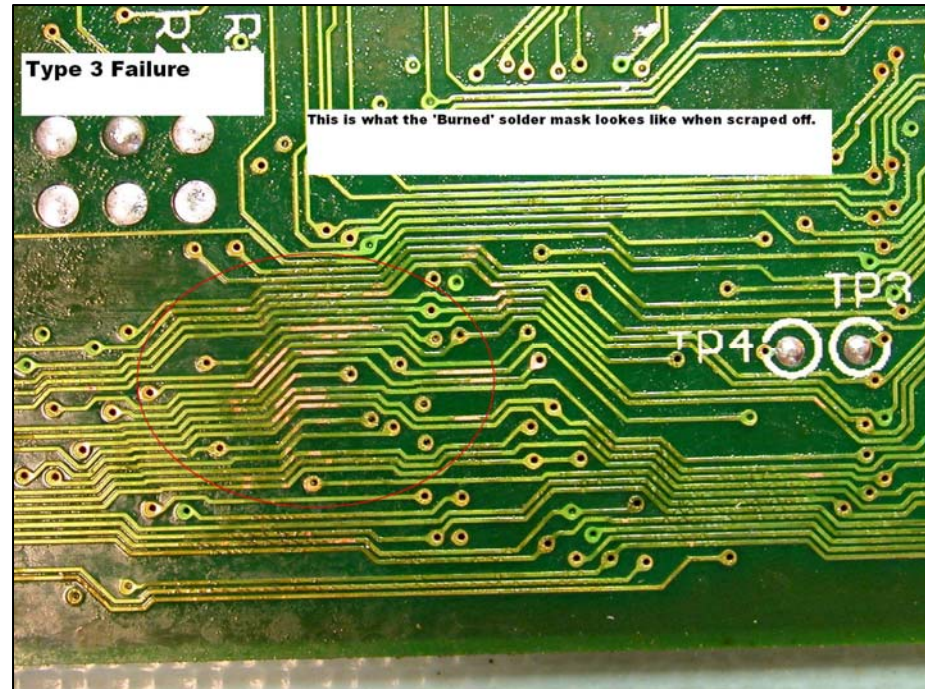
- Higher surface tension impact
- Flux dependent
- Solder temperature dependent
- Contact time dependent
- Finish dependent, copper worst



Voids in DIP IC Socket, NiAu PCB,
Tin plated leads, 1.4 meters/minute,
Solder 260°C, in air, ROL1 Flux

Mask Blistering

- ❑ Excessive solder temperature
- ❑ Excessive solder contact
- ❑ Mask curing incomplete
- ❑ Flux incompatibility
- ❑ Moisture entrapment

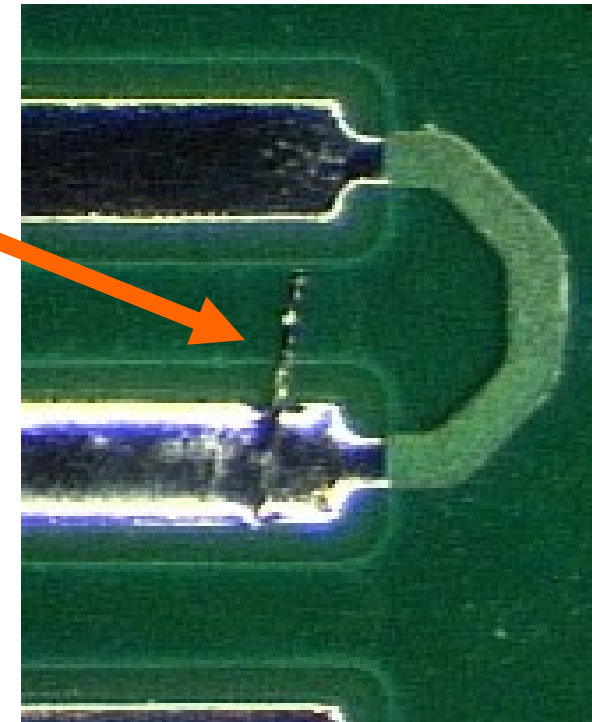
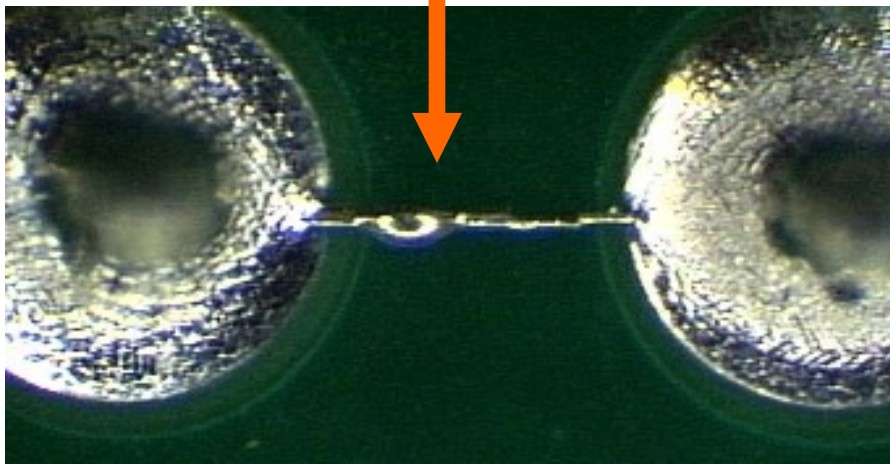


SAC305 solder was used in the above with a contact time of 5 seconds

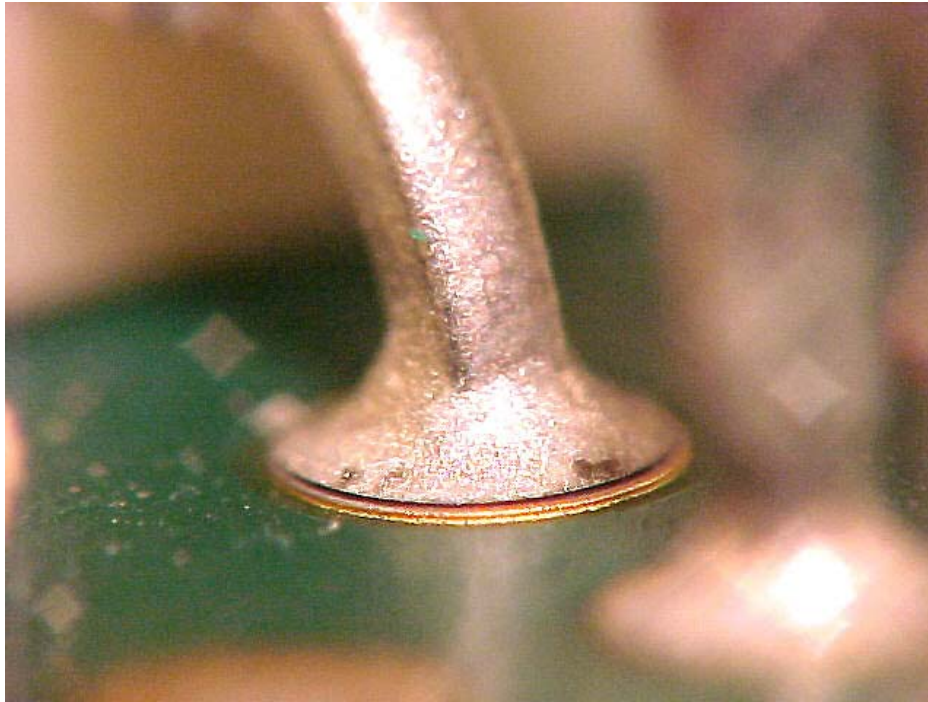
High Iron Contamination

- Formation of needles
- Surface tension effect

Tin-Iron needles intermixed with solder



Fillet Lifting



**SAC 305
Pad lift**

- Pad geometries
- Pb or Bi inclusions
- Not necessarily a defect as per IPC-610D



Lead-free Hand Soldering and Rework

Understanding the Process to Achieve Reliable Repeatable Results





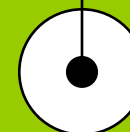
Hand-soldering Variables

- Alloy melting temperature
- **Soldering temperature requirements**
- Flux type - no clean, rosin, rosin free, water soluble
- Flux activation level
- **Flux percentage 2 or 3%**
- Flux volatility and flux spatter
- Cleanability of residues (if required)



Standard Core Sizes

Best Flux Percentages

Non-Standard	Standard	Standard	Standard	Non Standard
NO. 70 VERY LARGE	NO. 66 REGULAR	NO. 58 MEDIUM	NO. 50 SMALL	NO. 40 VERY SMALL
				
*4.5%	*3.3%	*2.2%	*1.1%	*0.5%

*Average weight percentage for LF and Sn60Pb40 alloy.

The average weight percentage will vary slightly depending on the density of the alloy.

Standard Wire Diameters

COMMONLY SPECIFIED DIAMETERS		
INCH	ENGLISH WIRE GAUGE EQUIVALENT	APPROXIMATE MM EQUIVALENT
0.125	11	3.17
0.093	13	2.36
0.062	16	1.57
0.050	18	1.26
0.040	19	1.02
0.031	21	0.78
0.025	23	0.63
0.020	25	0.50
0.015	28	0.40
0.010	31	0.25



Connection Temperature

- High enough to melt solder & form inter-metallic.
- High enough to activate flux & cause wetting.
- Low enough to avoid damage to components/PCBs

Too Low

INCREASING TEMPERATURE

Too high

- Cold solder joints
- Poor wetting
- Little intermetallic
- Large contact angles
- No reliability

- Good wetting
- Good contact angles
- Thin intermetallic layer
- Less oxidation
- Reliable joints

- Component damage
- Board damage
- Thick intermetallic
- Dewetting
- Reduced reliability

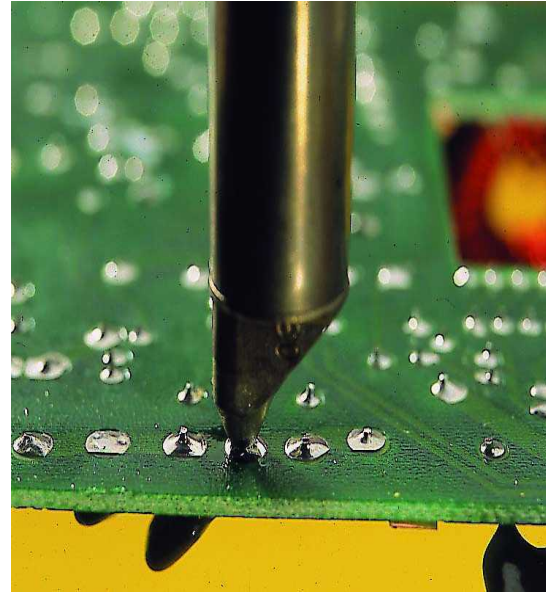
Tip Care: Choosing a Tip

- Select the largest tip possible
- Use the lowest possible temperature

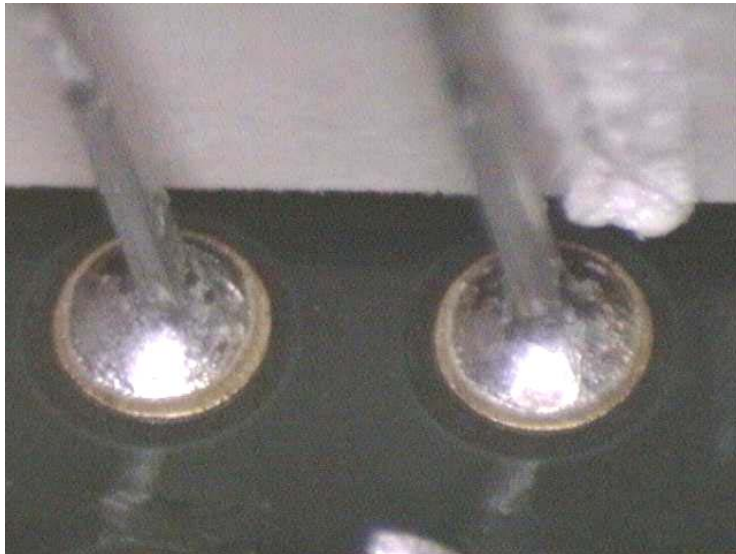


Correct Tip Selection

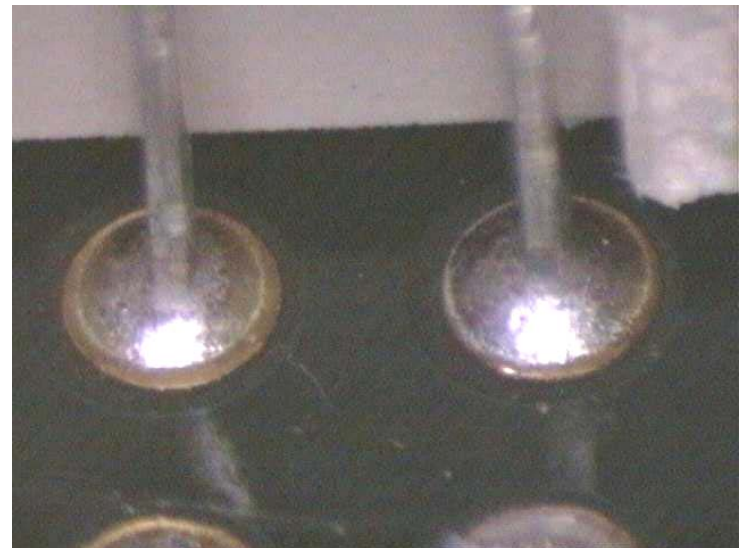
- Hole Size
- Pad Size
- No Pressure



Hand-Soldered Top side connector fillet, SAC Alloy

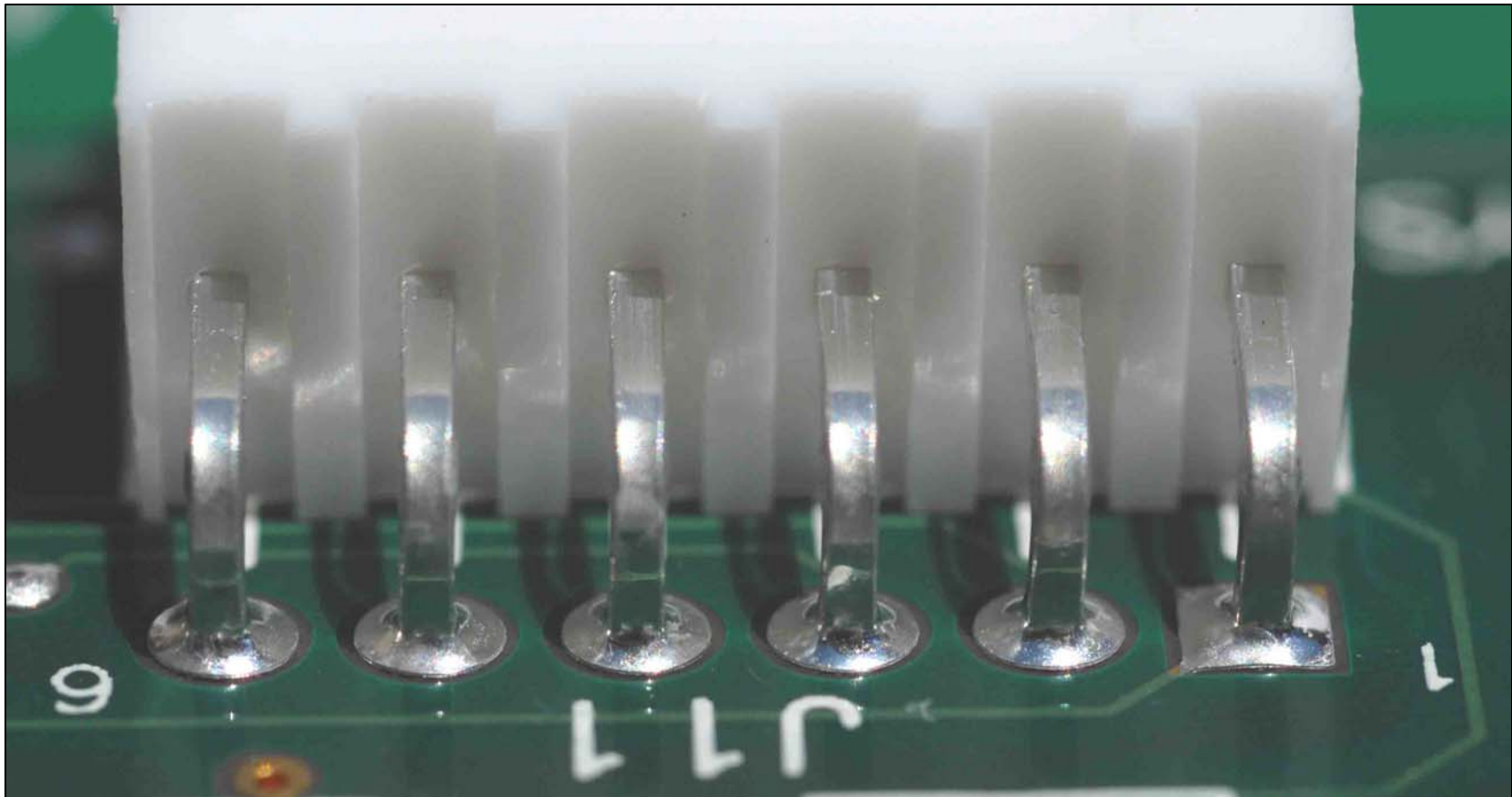


Lead finish SnCu



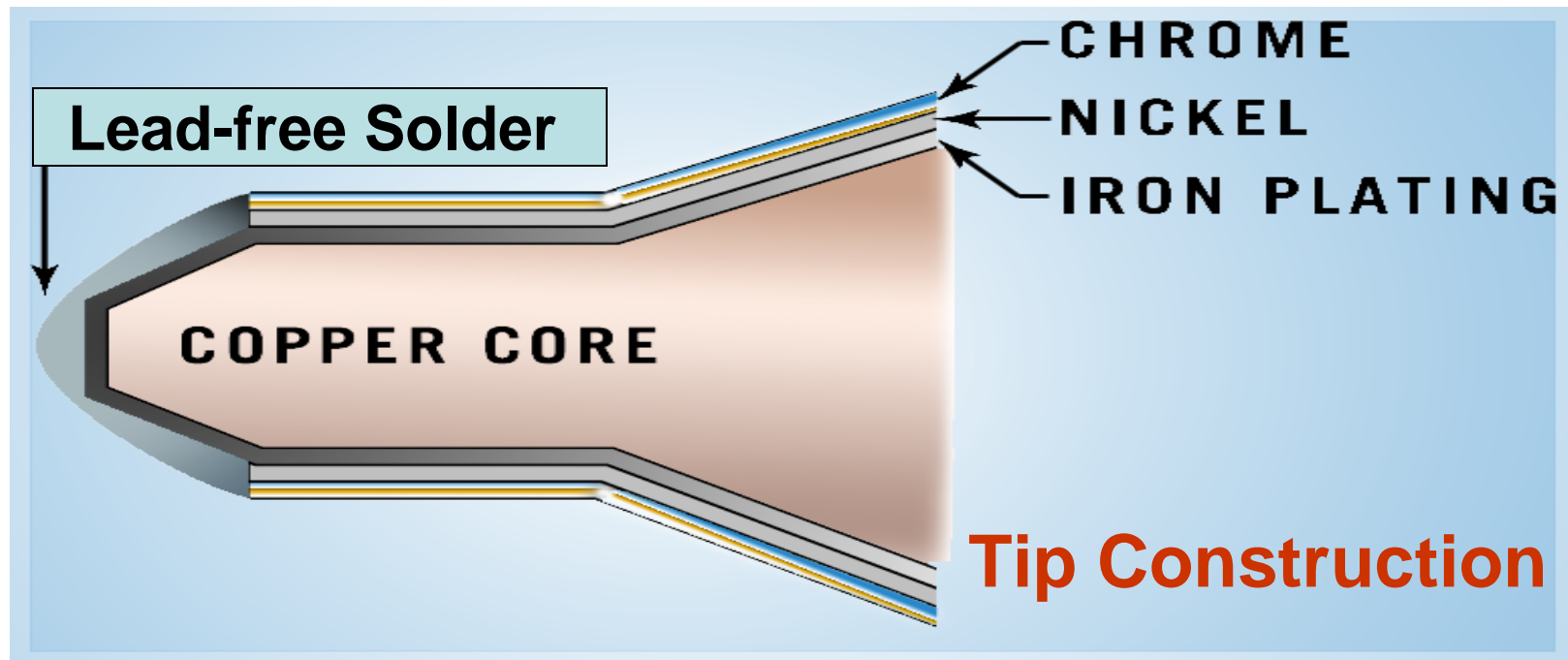
Lead finish Sn

K100 Solder Wire with 331 Flux, Hand-soldered Top-side J11 Connector



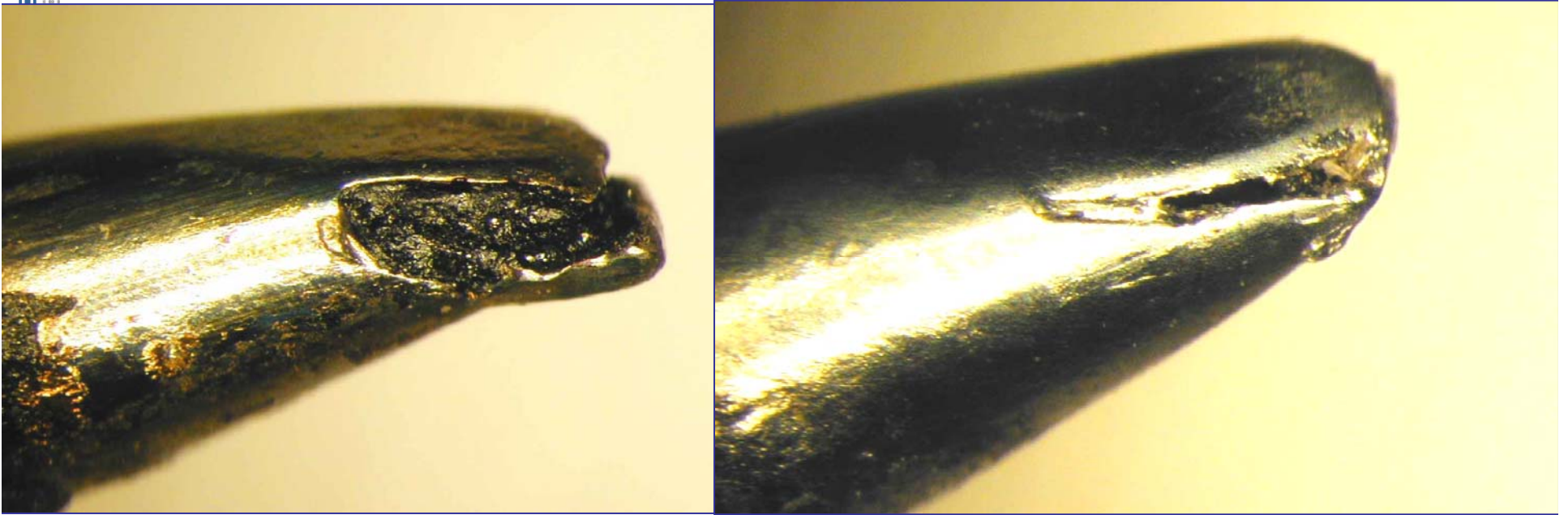
Excellent flow and no dullness; no shrinkage effects

The Issue with Tip Plating



For lead-free the tip is tinned with lead-free solder

Soldering Tip Erosion with Lead-free



Failure after 3 weeks, 120 hours; typically was 3 months

What causes Tip Failures - Summary Apex Conference 2006

FAILURE	CAUSE	EFFECTS	PREVENTION
Stress/Crack	Unnecessary Force Applied to Tip Mishandling	Iron Plating Cracks Solder Dissolves Exposed Solder Core	Select Proper Tip Use Tip as Designed
Abrasion	Scrubbing Tip with High Abrasives	Premature Wearing Away of Tip Plating Solder Dissolves Exposed Solder Core	Use De-Ionized Water Follow Proper Cleaning Procedures
Normal Wear	Normal Use		Use Clean, Sulfur-Free Sponges
Corrosion	Tip Tanners Used incorrectly Solder & Flux Interaction LEAD-FREE MORE AGGRESSIVE	Iron Plating Stripped Away ISSUE FLUX REQUIREMENT	Use Lower Activity (RMA) Fluxes (Opposite w/LF) Use Standard Solders for Tip Tinning Use Clean, Sulfur-Free Sponges
De-Wetting	Oxidation of Iron Plating	Solder Doesn't Adhere to Tip Reduced Heat Transfer	Clean & Tin Regularly Solder @ Lower Temps

Solder Products Differentiation

- Material control
- Easily identifiable
- Increases awareness
- Simplifies training
- Avoids costly errors
- Insures reliability





Thank-you

More info on any slide,
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